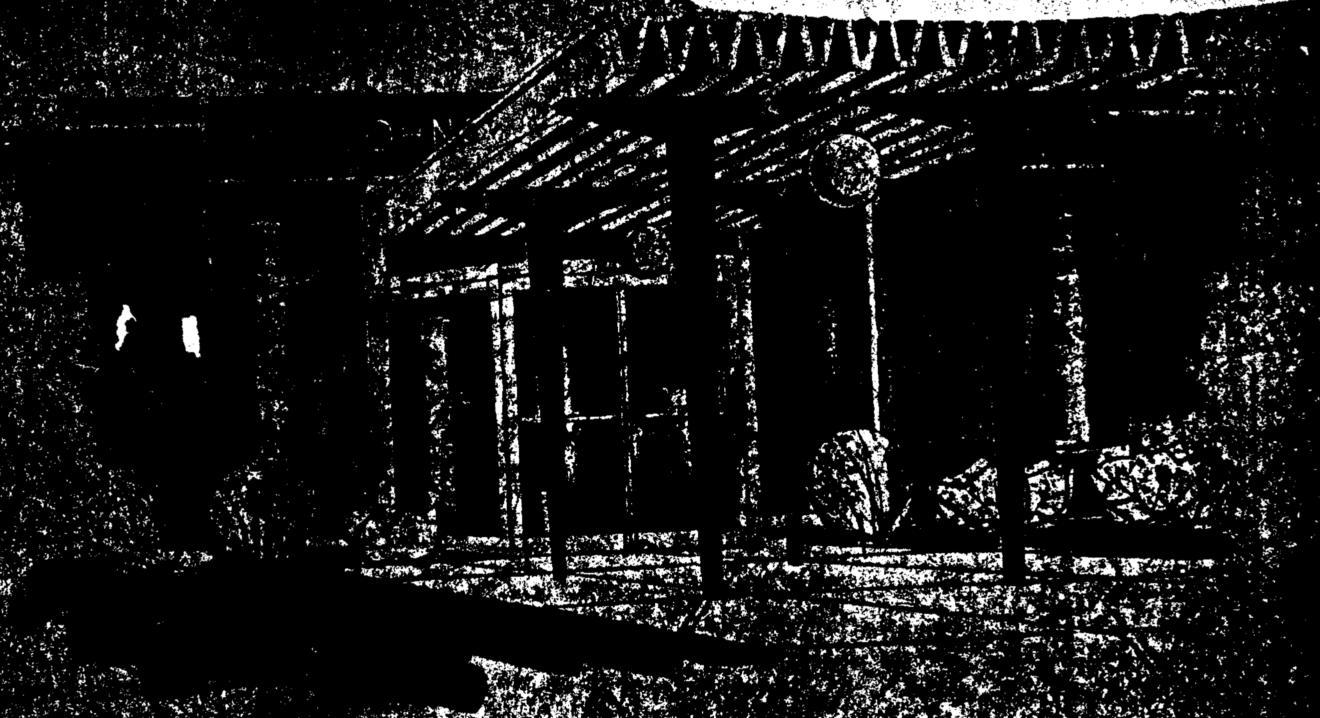
OPERATING MANUAL

VIKING VALIANT II TRANSMITTER



JOHNSON VIKING VALIANT II TRANSMITTER

Model 240-105-1 (Kit Form)
240-105-2 (Assembled and Tested)

OPERATING MANUAL CONTENTS

CONTENTS
Page 2

TABLES

ILLUSTRATIONS — Following Page 42

WARNING

The voltages encountered in this piece of equipment are high enough to cause fatal injury! Practice safety rules until they are second nature. Always turn off the high voltage before making any adjustment inside the transmitter. Never depend on a bleeder resistor to discharge filter capacitors. After the power is turned off, short circuit the high voltage circuit. Never operate the transmitter with any other than the recommended fuses in the primary circuit. The fuses will protect your equipment; in case of accidental contact with the high voltage, they may save your life. If children have access to the open transmitter, always disable the primary circuits by removing fuses, or the high voltage circuits by removing rectifiers. Always remove the line cord plug from the power source when working inside the transmitter.

A. INTRODUCTION

1. Function

The Viking Valiant II is a self contained radio frequency transmitter designed for amateur service. It may be used for CW telegraphy, AM modulated phone or, with a suitable exciter, SSB phone communication.

Approximate final amplifier ratings are:

Mode	Plate Power Input*	RF Output*
CW	275 watts	200 watts
AM	200 watts	150 watts
SSB		150 watts (P.E.P.)

The ranges of operating frequencies are:

1.75 mcs. to 2.0 mcs.
3.5 mcs. to 4.0 mcs.
7.0 mcs. to 7.42 mcs.
14.0 mcs. to 14.85 mcs.
21.0 mcs. to 21.6 mcs.
26.9 mcs. to 27.36 mcs.
28.0 mcs. to 29.7 mcs.

Maximum output power is essentially constant throughout the operating range.

2. Construction

The transmitter is 21 1/8" wide, 17 3/8" deep, 11 5/8" high; weighs 83 pounds net. A perforated cadmium plated steel cabinet and cadmium plated steel panel result in total enclosure with adequate ventilation.

All operating controls are located on the front panel, as well as the meter, frequency determining dial and pilot lamps. Microphone input jack, keying jack, phone patch input, auxiliary power receptacle, SSB input jack, RF output receptacle, relay jack and ground stud are located on the rear of the chassis.

To aid in eliminating spurious radiation which might result in interference to other services such as television broadcasting, the transmitter cabinet serves as an effective shield. Monel metal braid is used to bond the panel and seal all possible openings between the one-piece cabinet and panel. The meter is shielded at the rear and has individual RF filters in meter leads. All external connections such as power cord, microphone input receptacle, relay jack, etc. are equipped with individual RF filters to maintain cabinet shielding integrity.

Operating frequency is determined by the bandswitch and high stability temperature compensated, integral variable frequency oscillator, both controlled from the front panel. The oscillator is calibrated directly in output frequency and the illuminated dial provides calibration points in 10 KC increments throughout the frequency range.

Socket J7, located behind a dummy knob cover on the front panel will accommodate two crystals for spot frequency operation.

*maximum input dependent somewhat on power line voltage
(P.E.P.) peak envelope power

3. Auxiliary Equipment

Microphone - - For phone operation a crystal or high impedance dynamic microphone is required. The Valiant II is equipped with a low current DC "push-to-talk" relay requiring only a microphone with a "push-to-talk" switch to actuate it.

Key - - Any hand key, "bug" or electronic key available may be used for CW operation. The DC current thru the key is negligible and a keying relay is not required.

SSB Exciter - - For SSB phone operation the transmitter required approximately 3 watts of single sideband suppressed carrier excitation at the output frequency. This requirement is met by the Viking SSB Adapter and by a number of commercially available SSB exciters. The output frequencies available and quality of the SSB signal are dependent upon the design of the accessory exciter.

Antenna Coupler - - Unbalanced resistive antenna loads from 50 to 500 ohms impedance may be matched by the pi-network output tuning system. Antennas are easily designed to fall within this impedance range and an antenna coupler is not then required.

If it is required to work into two wire balanced antenna transmission line systems or to work into highly reactive antenna systems such as may be encountered by using one antenna for a number of different frequency bands, an antenna coupler such as the 250-23 JOHNSON "Matchbox" should be used. Alternative solutions to antenna matching problems may be found in the ARRL Handbook in the chapters "Transmission Lines" and "Antennas".

Low Pass Filter - - While the pi-network output circuit of the Valiant II provides good harmonic suppression, there are many locations where harmonic output must be reduced to an absolute minimum to avoid interference with "fringe area" television reception. In this case a low pass filter such as the 250-20 JOHNSON is a highly desirable accessory. Since a low pass filter is a fixed impedance device (52 ohms in the case of the 250-20) antenna impedance matching flexibility must be achieved by using an antenna coupler after the low pass filter.

4. Power Requirements

The Valiant II is designed to operate from a 117 volt, 50/60 cycle single phase AC line voltage source. Since the variable frequency oscillator and amplifier screen grid voltages are regulated, the equipment is substantially independent of line voltage regulation within the limits 105 to 125 volts. With 117 volts line voltage, power consumption is:

Standby	185 watts
Key down CW (fully loaded)	560 watts
Phone, fully loaded, speech modulation	560 watts (average peaks)

B. DESCRIPTION

1. Exciter

The Valiant II exciter section consists of a 6AU6 (V1) variable frequency oscillator, a 6CL6 (V3) crystal oscillator/buffer and a 5763 (V4) frequency multiplier/driver.

The primary method used to establish frequency control is the 6AU6 high stability electron coupled oscillator. The oscillator is voltage regulated and temperature compensated. Drift and frequency shift due to temperature rise or line voltage variation are negligible. The construction of these circuits is extremely rigid to minimize the effects of shock or vibration. The 6AU6 oscillator and its associated OA2 (V2) screen voltage regulator are housed in a separate compartment, carefully shielded and isolated from all other radio frequency circuits to avoid frequency modulation of the oscillator output.

The oscillator is equipped with two separate tank circuits, one covering the range 1.75-2.0 mcs. for output on the band 1.75-2.0 mcs. and 3.5-4.0 mcs. The other tank circuit covers basically the range 7.0-7.42 mcs. for all other output frequencies except the 11 meter band. Here the oscillator tunes the range 6.725 mcs. to 6.84 mcs. for output in the range 26.9-27.36 mcs. Oscillator tank circuits are selected by SW1 actuated from the shaft of the bandswitch SW3 by the drive arm D1 and the cam D2. Oscillator frequency is determined by the capacitor C1A, B driven by the main dial and planetary drive assembly D3.

Using VFO frequency control, the 6CL6 crystal oscillator/buffer serves as a broad banded amplifier/frequency multiplier and serves to further isolate the VFO from succeeding RF stages. The plate circuit is switched by SW3A, the deck of the bandswitch nearest the front of the transmitter.

With switch SW2 in the "C1" or "C2" position, the VFO is disabled by removing L19 from ground thus opening the cathode circuit of V1. At the same time, one of the crystals is connected by SW2 between the grid of V3 and ground. V3 then becomes a "hot cathode" crystal oscillator. In the "C1" position of SW2 a crystal connected between pins 3 and 5 of J7 is operative. In the "C2" position the crystal connected between pins 1 and 7 is in use.

With SW2 in the "VFO" position the cathode of V1 is grounded thru L19, the plate of V1 is connected to the grid of V3 thru the coupling capacitor C22 and the crystals are removed from the circuit.

These same conditions exist when SW2 is switched to the "zero" position plus the fact that SW2 grounds pin 7 of the 12AU7 keyer (V11) thus keying the whole exciter chain.

The 5763 buffer/multiplier (V4) employes a tuned high Q plate circuit operating on the same frequency as the final amplifier on all bands. The plate circuit is switched by SW3A, is tuned from the front panel by C7, the dial being marked "EXCITER". This stage is protected against excitation failure by the cathode resistor R60. The buffer switch and coils are shielded to guard against interaction with other circuits. R51 operated from the front panel and marked "DRIVE" controls the screen voltage of the 5763 thus controlling the excitation to the final amplifier.

2. RF Amplifier

This stage employs three 6146 tubes (V5, V6 and V7) connected in parallel. Layout and design is such as to provide high efficiency together with stability and freedom from spurious output. The high Q pi-network output circuit has good efficiency throughout the operating range and provides excellent harmonic suppression when operated into non-reactive loads of 50 to 500 ohms impedance. The range of antenna impedance which may be matched at frequencies above 7 mcs. extends, roughly, from 25 to 2,000 ohms. The output capacity switching assembly (C41, C42 and SW6) is arranged to avoid inductive loops coupling back to the preceding stages.

The inductance in the plate circuit of the amplifier is switched to change bands by means of the rear deck of SW3B. The amplifier is tuned to resonance by means of C8 operated from the front panel by the dial marked "FINAL". The knob of SW6, the coarse coupling switch, is marked "AUX COUPLING" the dial operating C9, the output coupling capacitor is marked "COUPLING FINE".

The 6AQ5 clamper (V8) is an integral part of the final amplifier circuit in that it protects the amplifier under conditions of no excitation. With the "MODE SWITCH" SW4, in either the CW or AM phone position, removal of excitation to the final amplifier, either by reason of keying or detuning of the exciter would cause the plate dissipation to rise prohibitively. Removal of excitation to the final amplifier eliminates the self bias generated at the grids of the 6146s causing the potential at the control grid of the 6AQ5 clamper to shift in a positive direction causing the clamper to draw current. Current flowing in the clamper plate circuit increases the drop thru the resistor R16 thus limiting the potential at the screen grids of the 6146s and the plate dissipation. With normal excitation to the amplifier the voltage at the grid of the clamper exceeds cutoff, the clamper then having no effect on the circuit.

To operate the Valiant II on SSB requires an SSB exciter capable of delivering 3 to 4 watts peak envelope power output at the desired operating frequency. Both the 5763 multiplier and the 6146 final amplifier tubes are used as linear amplifiers in this mode of operation. Provision is made to bring out VFO output for use with Viking SSB Adapter or any exciter requiring it.

3. Audio Section

The speech system consists of a 12AX7 (V12) cascade connected dual triode speech amplifier, 6AL5 (V13) diode audio clipper, 6C4 (V14) third audio amplifier, 12AU7 (V15) audio driver and push-pull 6146 (V16, V17) modulators.

Two audio inputs are provided. J1 on the rear of the chassis is the microphone input. Terminal 1 connects the audio output of either a crystal or high impedance dynamic microphone to the grid of the first audio stage. Terminal 2 and ground of J1 connect in parallel with SW8 and if a push-to-talk microphone is used, the switch in the microphone actuates the push-to-talk relay, RY1. The phone jack, J3, also on the rear of the chassis, serves as a phone patch input. It connects between cathode and ground of the second audio stage (V12B) and is in parallel with the cathode resistor, R29. This lead should be blocked by a 0.1 mfd. capacitor to prevent shorting of the cathode resistor by the phone patch circuit if such a capacitor is not part of the phone patch unit.

The audio clipper (V13) will provide up to 20DB of speech clipping, markedly improving the effectiveness of the transmitter signal. The audio filter following consisting of C94, C95 and L45, may be considered as a part of the clipper since it is used to correct the audio wave form after clipping. The filter also serves to limit the frequency response to the range 250 to 3000 cycles. Modulation level and degree of clipping are controlled by R34, the clipping level control on the front panel marked "CLIPPING", and by R28, the audio gain control mounted on the front panel and marked "AUDIO".

4. Power Supplies

Three supplies are used to power the Valiant II. The low voltage supply rated at a nominal 300 volts serves the exciter and speech system exclusive of the modulator. The power transformer is T2 and the rectifier a 5V4G (V20). A separate winding of T2 connected to the cathodes of the 6BY5GA rectifier (V21) serves to supply rectified bias of -265 volts to the transmitter.

The high voltage supply of 660 volts consists of the power transformer T1 and the 866A rectifiers (V18, V19). It serves to power the modulators and the final amplifier.

The low voltage supply and bias supply as well as all filaments are energized by switch SW7 located on the left side of the front panel and marked "FIL". The high voltage supply is energized by the relay RY1 actuated by either SW8 or by a microphone switch connected between pin 2 and ground of J1.

All supplies are protected by the 8 ampere 3AG power line fuses F2 and F3 located in the AC plug P9. A third fuse F1, 1.6 amperes 3AG is located inside the chassis on the rear edge. This fuse serves to protect the circuits associated with T2. These circuits are independent of amplifier loading and a failure of F1 is indicative of trouble which requires opening of the transmitter to service.

Two separate voltage regulation circuits are incorporated in the Valiant II. One circuit, an OA2 (V2) regulates the screen voltage of the VFO (V1) for maximum frequency stability. The second regulator circuit using two OC3/VR-105 tubes (V9, V10) holds the screen voltage of the final amplifier to close limits when operating the amplifier as a SSB linear amplifier. When the Valiant II is operated in the AM mode, thepair of VR-105s regulates the screen voltage of the 6146 modulators (V16, V17).

The receptacle J8 has been provided to permit the use of the Valiant II power supplies and modulator for other equipments such as a VHF transmitter. Removal of the shorting plug P8 from J8 disables the entire RF section by removing the filament voltage. J8 then has available at its terminals the output of the modulator, approximately 100 watts of audio, 6.3 volts AC at 9 amperes, 660 volts DC at 350 ma., 300 volts DC at 75 ma. The 660 volts DC may be taken out of the transmitter either modulated or as DC thus eliminating the necessity for external modulator wiring. Any associated equipment, used with the Valiant II powering it, is controlled by the Valiant II control system. If push-to-talk operation is to be used and a keying circuit is required then the output from J4 will operate a 110 volt AC relay to perform any required function.

Normal use for J4 is to supply 110 volts AC keyed by the relay RY1 to operate an antenna change over relay.

5. Panel Nomenclature and Control Functions

FIL - - Switch SW7, in the up or "on" position applies power to transformer T2 applying filament voltage to all tubes, plate and screen voltage to all stages except final amplifier and modulator. Applies fixed bias voltage to exciter stages, final amplifier, modulator and driver.

PTT-MAN - - Switch SW8, in the up or "Man" position applies power to T1 putting plate and screen grid voltage on final amplifier and modulator. SW8 does not function unless SW7 is "on". The up position is for manual control and the down position (PTT) is for push-to-talk relay control by means of the microphone push-to-talk switch.

METER - - Switch SW5, connects meter M1 to measure various transmitter currents:

SW5 Position	Current	Stage	Scale	Tubes
OFF	- - -	- - -	- - -	- - -
OSC	Cathode	Osc/Buffer	0 - 50	V3
BUFF	Cathode	Multiplier	0 - 50	V4
GRID	Grid	Final Amp.	0 - 25	V5, 6, 7
PLATE	Cathode	Final Amp.	0 - 500	V5, 6, 7
MOD	Cathode	Modulator	0 - 250	V16, 17

EXCITER - - C7, tunes the plate circuit of the multiplier, V4.

VFO - - C1A, B determines VFO frequency within the frequency band.

FINAL - - C8A, B tank tuning capacitor for final amplifier.

DRIVE - - R51, controls screen voltage applied to V4 thereby controlling excitation to final amplifier grids.

CLIPPING - - R34, audio clipping level control.

OSCILLATOR - - Switch SW2, selects either of two crystals or VFO frequency control. In the "zero" position, SW2 keys the exciter chain.

MODE - - Switch SW4, in the "CW" position grounds the screen grids of the modulators and short circuits the secondary of the modulation transformer. In the "AM" position applies regulated voltage to modulator screen grids, opens up the modulator transformer secondary short circuit. In the "SSB" position applies regulated screen voltage to the final amplifier, removes excitation from V3 to multiplier V4, disables modulator and connects the SSB exciter output to the multiplier input circuit.

CRYSTALS - - Dummy knob conceals socket J7 accommodating two FT243 type crystal holders. Crystal C1 plugs into socket terminals 3 and 5, crystal C2 into socket terminals 7 and 1.

BAND - - Switches SW1 and SW3, selects VFO tank circuit and determines tuning range of succeeding exciter stages and final amplifier.

AUX COUPLING - - Switch SW6 adjusts the output coupling capacity of the final amplifier pi-network by selecting fixed mica capacitors.

COUPLING FINE - - C9, variable air dielectric capacitor, a component of the pi-network output circuit. This capacitor together with fixed mica capacitors provides a continuously variable output loading capacitor.

AUDIO - - R28, 1 meg potentiometer adjusts audio input to the second audio stage, determines modulator output level.

C. INSTALLATION

1. Unpacking (factory wired transmitter)

After removing the transmitter from its shipping container, inspect it thoroughly for any possible damage from shipping. Claims against the carrier delivering the equipment must be made with the carrier's agent at the point of delivery. DO NOT SHIP DAMAGED EQUIPMENT BACK TO THE MANUFACTURER UNTIL AUTHORIZED TO DO SO BY THE MANUFACTURER. NOTIFY THE SERVICE DIVISION THAT A CLAIM IS BEING MADE AGAINST THE CARRIER.

In order to attach the knobs, install tubes and remove packing material it will be necessary to remove the transmitter from the cabinet as follows:

a. Loosen and remove the four tie bolts which are located at the top, left and right ends of the rear of the cabinet.

b. Loosen and remove the screws around the periphery of the cutout located on the rear of the cabinet.

c. Slide the chassis out of the cabinet carefully, training the line cord thru the large opening.

Remove the packages containing the knobs and the four plugs, P8, a nine pin plug with cover; P3, a phono plug; P4, antenna relay plug; and P10, a 5 pin jumper plug.

Remove the packing from around the final amplifier coil and any additional packing inside the cabinet and on the chassis.

Remove the supports provided underneath the chassis on the transformer mounting screws.

Install any tubes which are separately wrapped. Refer to Figure 1 for locations and Figure 9, the schematic diagram, for the tube type numbers corresponding to the "V" numbers appearing on Figure 1. V1 and V2 will already be installed in the VFO compartment.

Check to see that all plate cap connectors are in place.

Replace transmitter in cabinet after performing all tests and operation is normal.

2. Installation of Knobs

Install knobs as follows (set screws for all knobs are shipped separately and are installed at time of mounting).

Install the large 2 3/8" knob, using one 10-32 set screw, on the 1/4" shaft extending from the VFO planetary drive, being careful not to permit the knob to rub the VFO dial escutcheon. Tighten the set screw.

Directly below the VFO dial knob, install the 1 5/8" knob on the "BAND" switch shaft extension using two 8-32 set screws. Set the switch to the maximum counter-clockwise position and set the knob marker to coincide with the 160 meter mark. Tighten the set screws.

Install one of the 0-100 dials on the shaft marked "EXCITER". Adjust the dial to "O" with capacitor C7 fully meshed. Tighten the 8-32 set screw.

Install the remaining 0-100 dial on the shaft marked "FINAL". Adjust the dial to "O" with the ganged capacitor C8A, B fully meshed. Tighten the 8-32 set screw.

Install the balance of the knobs using 8-32 set screws as follows:

Panel Nomenclature	Shaft Position	Knob Marker Position
METER	counter-clockwise	"Off"
OSCILLATOR	counter-clockwise	"C1"
MODE	counter-clockwise	"CW"
AUX COUPLING	counter-clockwise	"O"
FINE COUPLING	C9 meshed	"O"
AUDIO	counter-clockwise	"O"
DRIVE	counter-clockwise	"O"
CLIPPING	counter-clockwise	"O"

Check the function of each knob to see that the indexing agrees with the marking on the panel (i.e. BAND switch on 160 meters with the switch at the counter-clockwise position and 11 meters when fully clockwise).

3. Bias Adjustment (adjust only if static modulator current is other than 50-70 ma).

NOTE: The operation of this equipment involves the use of high voltages dangerous to human life. Use extreme care and caution.

Turn the clamper potentiometer R13 (located to the right of V8) to its full clockwise position.

Check to see that both of the 8 ampere fuses are installed in the line cord plug.

Check to see that P8 is installed in J8 on the rear of the chassis.

Check to see that P10 is installed in J9 on the rear of the chassis.

CAUTION: Plug P10 MUST be inserted in J9 at all times when SSB operation is not contemplated.

With switches SW7 (marked FIL) and SW8 (marked MAN-PTT) both off (down) insert plug into 117 volt line.

Bias voltages for the modulator and final amplifier are established by means of the two potentiometers, R61 and R62. They are located on the side of the chassis near socket XV21. These adjustments have already been made on factory wired transmitters. Access has been provided by means of two holes in the side of the cabinet.

For finish adjustment set transmitter controls:

Control	Position
MODE	CW
DRIVE	0
PTT-MAN	PTT (OFF)
FIL	On
AUDIO	0

Final amplifier grid voltage should be -69 volts negative with respect to ground. Set the potentiometer R62 for -69 volts amplifier grid voltage (measure at either end of L7 and ground).

To adjust the static modulator current, turn the potentiometer R61 to the extreme counter-clockwise position. Connect a dummy load to J6 and set the controls as follows:

Control	Position
BAND	80
VFO	3.5
MODE	AM
OSCILLATOR	VFO
METER	Grid
FIL	On
PTT-MAN	PTT (OFF)
AUDIO	0
COUPLING	1 AUX., 0 FINE
DRIVE	2
CLIPPING	0

Switch the OSCILLATOR CONTROL to ZERO and tune EXCITER CONTROL for maximum drive. Adjust DRIVE CONTROL for 8 ma. grid drive and return OSCILLATOR CONTROL to VFO. Turn METER SWITCH to Plate Position, switch PTT switch to MAN and resonate the final. Load the final up to 330 ma. and recheck grid drive. It should be 8 ma. Turn meter switch to MOD position. Adjust static modulator current to 60 ma. by slowly turning R61 clockwise.

These adjustments should result in operating conditions of 50-70 ma. static modulator current on AM phone, approximately 100 ma. static amplifier plate current on SSB operation.

4. Clamper Adjustment (adjust only if final key up current is other than 5-15 ma.)

The clamper is used to reduce screen voltage automatically under conditions of no excitation of the final amplifier. It is adjusted by means of R13, a potentiometer with slotted shaft located near the rear of the chassis next to the clamper tube V8 (6AQ5). This adjustment need be made only once, should be re-checked when changing V8, the 6AQ5 clamper or the 6146 tubes in the final amplifier.

Set up transmitter controls as follows:

Control	Position
METER	Plate
OSCILLATOR	C1 (no crystals in crystal socket)
MODE	CW
FIL	On
PTT-MAN	PTT (OFF)
AUDIO	0

R13 was previously turned to the full clockwise stop. Throw PTT-MAN to "MAN" position (On). Using an insulated screwdriver turn R13 slowly counter-clockwise until plate current just begins to rise. Set R13 for 10 ma. static plate current. Turn switch to PTT position (Off). BE CAREFUL, DO NOT GET ACROSS THE HIGH VOLTAGE!

5. Operational Checks

a. Position the controls as follows:

Control	Position
VFO	3.5 mcs.
METER	Osc.
MODE	CW
OSCILLATOR	VFO
BAND	80
COUPLING	3 AUX., 0 FINE
DRIVE	0
AUDIO	0

Settings of other controls are not important at this time.

Turn FIL to "On" position and allow transmitter to warm-up for a few minutes.

"Osc" current should read approximately 24 ma. (multiply bottom meter scale reading by two).

"Buff" current should read approximately 13 ma. (twice reading of bottom scale). Turn DRIVE control to 3 and note that "buffer" current will rise to about 22 ma.

Turn METER switch to "grid", tune EXCITER dial for maximum current with DRIVE at position 3.

Adjust DRIVE control for 8 ma. grid current (bottom meter scale).

Turn METER switch to "Plate", turn PTT-MAN to "Man" position and tune FINAL dial for minimum current. By adjusting the loading controls the plate current can be increased from less than 100 ma. to over 300 ma. as read on the upper meter scale. Turn switch off, (PTT position).

b. Turn controls as follows:

Control	Position
VFO	7.33 mcs.
OSC	VFO
MODE	CW
BAND	40
COUPLING	6 AUX., 0 FINE
DRIVE	5
AUDIO	0

Tune EXCITER dial for maximum grid current.

Adjust DRIVE control for 8 ma. grid current. Turn meter switch to PLATE and turn PTT-MAN to "MAN" position (on), tune FINAL dial for minimum current (on the top scale). Turn PTT-MAN off (PTT position).

c. Turn controls as follows:

Control	Position
VFO	28.6 mcs.
OSC	VFO
MODE	CW
BAND	10
AUX COUPLING	0
DRIVE	5
AUDIO	0

Tune EXCITER dial for maximum grid current. If necessary to obtain a reading, advance DRIVE control beyond 5.

Adjust L5, the screwdriver adjustment to the left of the VFO (beside the shaft of C7), for maximum grid current. (This adjustment will remain unchanged).

d. Set VFO at 27.125 mc. BAND on 11. Adjust L16 by squeezing or spreading turns, for maximum grid current. NOTE: If 12 ma. or more grid current is obtained with DRIVE at position 10, L16 need not be adjusted.

6. Keyer Adjustment

The keyer control R39 is a potentiometer with slotted shaft located to the left of and slightly to the rear of V3 (6CL6). Plug a key into J2. Set transmitter controls:

Control	Position
OSCILLATOR	VFO
FIL	On
MODE	CW
DRIVE	0
AUDIO	0
PTT-MAN	PTT (Off)

Set bandswitch and VFO to any convenient receiving frequency. Close key and tune the receiver to the VFO frequency. If more signal is required, turn the DRIVE control to 2 and tune EXCITER dial for maximum received signal. Open the key. Rotate R39 to the full clockwise position. This will key the VFO. Now turn R39 slowly counter-clockwise until the VFO drops out of oscillation. Do not leave the keyer adjustment at exactly the point where the VFO drops out of self sustained oscillation. Turn R39 counter-clockwise slightly beyond this point otherwise VFO instability can result.

D. 1. Accessory Connections

The possible connections to auxiliary equipment provided in the Valiant are listed below. The ones actually used depend upon the modes of operation and optional equipment utilized.

Accessory	Connector	Cable	Connections
Microphone	P1 (80-MC2M Amphenol)	2 conductor shielded (furnished with microphone)	To P1 connect; audio lead from microphone to pin 1, switch lead from microphone to pin 2, shield braid to shell. Insert P1 into J1.
Key	P2 (75 Mallory or equal)	2 conductor unshielded	To P2; connect one lead to each terminal. Insert P2 into J2.
Antenna	P6 (83-1SP Amphenol)	Optional	If coaxial cable is used to connect antenna; center condr. to center pin of P6, shield braid to shell. If single lead is used connect to center pin of P6. Insert P6 into J6.
Antenna Relay	P4*	2 conductor unshielded	Connect one lead to each terminal of P4. Insert into J4. Note that this circuit delivers 115V AC keyed by relay RY1.
Phone Patch	P3*	Single conductor shielded	Connect center conductor to center pin of P3, shield to shell. Insert in J3.
SSB Input	P5 (83-1SP Amphenol)	RG59/U	Center conductor to center pin of P5, shield to shell. Insert in J5.
Accessory Power	P8*	user's option	P8 is normally wired to complete heater and modulator output circuits when the transmitter is operated. Insert into J8. Refer to special instructions for using accessories such as the Viking 6N2.
Accessory Jumper Plug	P10*		P10 is required to permit AM and CW operation of Valiant II. Refer to section D9 for SSB operation.

* Furnished with the Valiant

2. VFO Checks

Wired transmitters leave the factory with VFOs calibrated and there is little danger of calibration changing. However, many times the operator will depend inadvertently on oscillator calibration to insure operating within band limits and for this reason VFO calibration should be checked at band edges.

One method of checking VFO calibration is to use a communications receiver as a detector. The frequency standard such as an LM type frequency meter, 100KC crystal calibrator or other standard should be fed into the receiver at a level which will not block the receiver yet produce a strong enough beat with the BFO to be easily detected.

The transmitter can be set up as follows:

FIL	On
OSCILLATOR	VFO Position
MODE	CW Position
DRIVE	0 Position

It is not necessary to tune any of the stages other than the VFO. Run a lead from the center contact of J6 letting it lie near the receiver antenna terminals. Adjust the lead position so as to provide a signal of approximately the same level as the calibrator.

With the Valiant II bandswitch in the 160 meter position beat the VFO with the calibrator at the calibration check points nearest 1.75 mcs. first, then nearest 2.0 mcs. These checks may be made at 3.5 mcs. and 4.0 mcs. if desired. The receiver BFO should be turned off, the beat between calibrator and VFO providing the audible check. The transmitter bandswitch may be in either the 160 or 80 meter position.

Next turn transmitter bandswitch to the 40 meter position. Compare VFO frequency with the calibrator as follows:

VFO Actual Oscillating Freq.	VFO Dial Reading	Frequencies Thus Checked
7.0 mcs.	7.0 mcs.	7.0 mcs.
		14.0 mcs.
		21.0 mcs.
		28.0 mcs.
7.15 mcs.	21.450 mcs.	21.450 mcs.
7.175 mcs.	14.350 mcs.	14.350 mcs.
7.425 mcs.	29.7 mcs.	29.7 mcs.

If it will simplify checking frequency, the receiver and calibrator may be operated on the frequencies indicated by the VFO dial. Checks will then be made against oscillator harmonics.

If a 100KC standard is the frequency comparison device there is no way to check such frequencies as 14.35 mcs. or 21.45 mcs. directly using audible beats. It becomes necessary then to check against the 100KC standard harmonics (multiples of 100KC).

To check 14.35 mcs., set the VFO to the 40 meter position, the VFO dial to 14.3 mcs. and the receiver to 14.3 mcs. The second harmonic of the VFO will then beat against the 143rd harmonic of the 100KC standard. Next tune the receiver and the VFO dial to 14.4 mcs., beating the VFO second harmonic against the 144th harmonic of the crystal calibrator. If calibration is accurate at 14.3 mcs. and at 14.4 mcs. then it can be assumed that the VFO calibration at 14.35 mcs. is quite accurate. The same technique can be used to check 21.45 mcs.

Turn bandswitch to 11 meter position and perform the following checks:

VFO Actual Oscillating Freq.	VFO Dial Reading	Frequencies Thus Checked
6.74 mcs.	26.960 mcs.	26.960 mcs.
6.8075 mcs.	27.230 mcs.	27.230 mcs.

If these checks disclose discrepancies in VFO calibration and if the calibrator used is known to be .005% accurate or better, then the VFO should be recalibrated per the instructions appearing later in this manual.

3. Tuning Procedure

NOTICE! The regulations of the Federal Communications Commission require a suitable license for operation of this equipment. Refer to publications of the Federal Communications Commission or the American Radio Relay League for the latest rules governing station and operating licensing.

Be sure to return the enclosed warranty registration card. This will register your transmitter at the factory. If it becomes necessary to write to the factory regarding your transmitter, refer to it by serial number.

The tuning procedure for the Viking Valiant II is identical on all bands of operation, 160 thru 10 meters. Therefore, the discussion of tuning on one band will apply to all bands. Only the dial and switch settings will change when going from one band to another. A 100 watt or larger bulb should be used for a dummy load, connect the dummy load between the center conductor and shell of J6. Connect a ground lead to the stud adjacent to J6.

See the Valiant II Control knobs:

Panel Nomenclature	Position
FIL	Down (Off)
METER	Off
MODE	CW
BAND	40
VFO	7.05 mcs.
AUX COUPLING	6
COUPLING FINE	0
DRIVE	0
AUDIO	0
CLIPPING	10
MAN-PTT	PTT (Off)

Insert the AC plug into 117 VAC 60 CPS receptacle. Turn FIL switch (SW7) "ON" Permit transmitter to warm up two minutes or more.

Turn METER switch to "OSC", note that the oscillator is drawing current. Turn METER switch to "BUFFER".

Turn OSCILLATOR switch to "ZERO" thus keying the transmitter. Note that the buffer now draws a slight amount of current.

Turn DRIVE control to 3.

Turn METER switch to "GRID", tune EXCITER dial for maximum grid current. Adjust grid current to 8 ma. by turning DRIVE control.

Turn METER switch to "PLATE".

Immediately after throwing SW8 to "MAN" position (ON) tune final dial for minimum current (resonance).

a. Output Loading on 10, 11 and 15 Meters

When starting to load the Valiant II transmitter on 10, 11 and 15 meters the AUXILIARY coupling control should be placed on position "9" and the FINE coupling control placed on "0". In almost all cases, the recommended FINAL plate current (450 ma. CW, 330 ma. PHONE) will be obtained with the AUXILIARY control in position "10" with full loading range obtained with the FINE control. However, it is desirable to load the transmitter from an unloaded position which is the reason for starting from position "9".

AUXILIARY coupling control position below "8" should not be used on 10 and 11 meters as there is danger of false loading and resultant high circulating currents of destructive magnitude.

The AUX coupling control should be set one number lower than shown in TABLE 4 (Typical Dial Settings on page 36 of the Operating Manual) when starting to load the Valiant II on 160, 80, 40 and 20 meters. The FINAL, AUXILIARY and FINE control settings may vary from those shown in TABLE 4 due to variation in antenna loads. The charted settings were obtained with a 50 ohm resistive output load.

Load amplifier by advancing AUX COUPLING switch a step at a time in a clockwise direction, retuning FINAL dial for resonance after each switch change.

As the amplifier approaches normal loading, 450 ma. for CW operation, 330 ma. for AM phone operation, complete loading of the amplifier by means of the COUPLING FINE control. Advance the COUPLING FINE control in a clockwise direction in small increments retuning to resonance each time with the FINAL dial.

Readjust DRIVE control for 8 ma. grid current.

Return OSCILLATOR switch to VFO position opening the key.

NOTE: Improper neutralization is very likely to become evident when loading the amplifier and adjusting grid current. Bringing the grid current up to the normal 8 ma. will cause the amplifier plate current to rise beyond the normal value. Reducing the amplifier loading will then cause the grid current to fall off. The net result of improper neutralization is to make it almost impossible to load the amplifier to the proper 330 ma. of 450 ma. while maintaining recommended 8 ma. grid current. Refer to neutralization covered in section D. 4.

4. Neutralization (adjust only if amplifier appears to be unneutralized)

The power amplifier of the Valiant II is neutralized by the double spaced variable capacitor C74 mounted in the corner of the shield SH1.

CAUTION! THE NEUTRALIZING CAPACITOR HAS FULL PLATE VOLTAGE APPLIED TO IT. ADJUSTMENT SHOULD BE MADE WITH AN INSULATED SCREWDRIVER.

Tune up the transmitter at any convenient frequency on the 20 meter band and load the amplifier to about 250 ma. with the dummy load. Note the exact reading of the FINAL dial where resonance (minimum plate current) occurs.

Turn meter switch to the grid position. Detune the final dial slightly in the direction which causes grid current to increase. (Don't move FINAL dial far nor leave the amplifier out of resonance very long because plate current increases rapidly and plate dissipation becomes prohibitive.)

If an increase in grid current occurs with a decrease in FINAL dial reading, the neutralizing capacity is too great.

If an increase in grid current occurs with an increase in FINAL dial reading, the neutralizing capacity is too small.

Adjust C74 in the direction indicated, return amplifier to resonance. While observing grid current, detune FINAL dial again in the direction causing grid current to rise. Repeat this step as necessary.

The amplifier is neutralized when detuning the FINAL causes little or no change in grid current or when detuning the FINAL dial in either direction causes grid current to fall off. Neutralization occurs with C74 at about 1/4 of maximum capacity.

5. Notes on CW Operation

The final amplifier should be loaded up to 450 ma. current indicated on the "plate" position of the METER switch. Grid current should be 8 ma. indicated on the "grid" position of the meter switch. Bear in mind that in the special condition where PTT-MAN is in the PTT or Off position but the exciter is keyed or the OSCILLATOR switch is in the "zero" position, grid current can rise several milliamperes over the value established when the amplifier is "On" and loaded.

An antenna changeover relay may be operated by the 115V AC power furnished by J4 when PTT-MAN is in the "man" or "ON" position. This mode precludes the use of full break-in operation.

To operate full break-in requires either the use of a separate receiving antenna or a TR box. Under these conditions, PTT-MAN is left "On" while operating.

To "zero beat" another station, turn PTT-MAN off then turn the OSCILLATOR switch to the "zero" position. With PTT-MAN On, the "zero" OSCILLATOR position keys the entire RF section of the transmitter.

6. Notes on AM Phone Operation

Nominal input to the final amplifier is 330 ma. on phone. With speech modulation and peak modulator current running approximately 165 ma., 100% modulation is achieved. The "no signal" static modulator current runs between 50 and 70 ma. (modulator current is read on the middle 250 ma. meter scale.)

Typical Values - AM Phone Operation

I_k - Amplifier - 330 ma.
I_g - Amplifier - 8 ma.
I_k - Modulator (static) -50-70 ma.

The operator has two choices in controlling the transmitter carrier. The carrier can be switched manually using the MAN-PTT switch or with a microphone switch to provide push-to-talk operation. The switch leads are connected between terminal 2 and the shell of P1. P1 plugs into J1 on the rear of the chassis. Either type of operation will actuate a 115 V AC antenna relay connected to J4.

7. Clipping Level Adjustment

The desired amount of speech clipping can best be established by means of a cathode ray oscilloscope, however an alternate method also follows. The oscilloscope should be set up to check for 100% modulation. (Information on hook-up and scope patterns may be obtained from the ARRL handbook). Set the AUDIO gain control R28 at "0", the CLIPPING control R34 in the full clockwise position. Put the transmitter in operation normally loaded for phone operation. While talking in the normal tone of voice used for communication with the microphone in its regular position, advance the AUDIO control until 100%

modulation is achieved on modulation peaks. While continuing to talk into the microphone, turn the CLIPPING control counter-clockwise until it is observed that modulation peaks are being slightly clipped. This serves to establish the threshold of clipping at 100% modulation.

The alternate method of adjusting clipping requires that the operator be able to talk into the microphone at a fairly constant amplitude and that he keep the same distance from the microphone.

Turn the CLIPPING control to the full clockwise position. Load the final amplifier to 330 ma. current with 8 ma. drive. While talking into the microphone at as constant level as can be maintained, turn the AUDIO control clockwise until the meter reads peaks of 175 to 200 ma. in the MOD position. Next turn the CLIPPING control to the full counter-clockwise position. Talk into the microphone at the same level as before turning the clipping control slowly clockwise until modulator current again reaches 175 to 200 ma. peaks. LEAVE THE CLIPPING CONTROL IN THIS POSITION. The clipping control setting will be approximately at 2 to 3.

Now refer to the curve "audio gain control position", Figure 11. Find the point on the curve corresponding to the present setting of the AUDIO control. Refer to the left side of the chart and determine the "relative gain DB" at this point on the curve. If 10 db of clipping is desired, add 10 to the relative gain figure just obtained. Project this new figure over to intersect the curve and read the AUDIO gain position indicated. Turn the AUDIO control to this new position. This setting will give 10db of clipping.

As an example, let us suppose that the setting of the audio which provided 100% modulation is 5. This point is 78db on the relative gain scale. Ten db added to this is 88db which corresponds to a new AUDIO gain setting of between 6 and 7 for 10db of clipping.

It may be noticed that the oscilloscope will indicate some overmodulation under these conditions. This results from phase shift as clipped wave forms pass thru the filter and modulation transformer. In well designed transmitters, this slight effect will not be detrimental. If desired, this effect can be eliminated by adjusting the CLIPPING control. Turn the CLIPPING control in a counter-clockwise direction slightly and check modulation. Repeat as necessary until overmodulation is eliminated.

8. Clipping Effects

Clipping is useful in overcoming interference but the recognizability of the operator's voice decreases as more clipping is used. Generally 10 to 12 db of clipping is the maximum desirable. The background noise present limits the amount of clipping which can be effectively used. A condition of high background noise together with excessive clipping will result in a nearly 100% modulation of the carrier by the noise thus obscuring the operator's voice and reducing intelligibility.

The following tabulation of the effects of speech clipping should aid in selecting the clipping level to be used.

6 db peak clipping - - clipping is barely detectable

12 db peak clipping - - not at all objectionable, on the contrary, speech sounds as though the speaker is enunciating with special care.

15 db peak clipping - - begins to interfere somewhat with the recognizability of the speaker.

19 db peak clipping - - speech sounds somewhat sharp and rasping but less unnatural than speech over a throat microphone.

24 db peak clipping - - speech quite intelligible but sounds unnatural and grating.

9. Notes on SSB Phone Operation

When the MODE switch SW4 of the Valiant II is turned to the SSB position, regulated screen voltage is applied to the final amplifier and a 50 ohm loading resistor is connected between grid and ground of V4, the 5763 multiplier stage. The 6CL6 stage (V3) is completely disabled by grounding the plate (for RF) and the screen. The SSB input jack J5 is also connected to the 5763 grid. The VFO output is available at J10.

The Viking Valiant II was specifically designed for use with the Viking SSB Adapter so all necessary interconnections are made when it is used. However when other adaptors are used with the Valiant II it will be necessary to remove P10 from the rear and connect it as shown in Sec. H3 in order to key the VFO and switch the bias voltages from standby to operate. The use of the Valiant II with the Viking SSB Adaptor is described in the Adaptor Operating Manual.

While the 50 ohm resistor (R10, R54 in parallel) from grid to ground will load the exciter considerably, it may be necessary to further dissipate exciter output. Operating the SSB exciter near or at full output will insure maximum attenuation of noise, hum and the suppressed sideband.

In SSB operation it is important that the final amplifier be loaded properly. When the loading is too light the amplifier is driven into saturation prematurely and the output is considerably reduced. If the coupling is too tight, saturation is no problem but the output will be below that of proper coupling. To establish correct loading the transmitter should be tuned up at the anticipated operating frequency with SW4 in the CW position. The final amplifier should be loaded up to 450 ma. plate current to the final amplifier using the regular CW tuning procedure and with normal grid current. Both EXCITER and FINAL TUNING WILL BE LEFT UNCHANGED FROM THIS POINT ON. Turn SW8 Off, throw MODE switch to the SSB position. Throw SW8 back On, adjust the DRIVE control so that with the meter in the "buffer" position, static current of the 5763 is 25 ma. Apply SSB excitation (at the same frequency as tuned in the CW mode) to J5 of the Valiant II. With voice modulation, increase the SSB exciter audio gain until the meter, in the "grid" position barely flicks upward on voice peaks. (Peaks as high as 1/2 ma. would be indicative of serious overdrive.) Turn the meter switch to the "plate" position. Depending upon the operator's voice and the waveform of the audio form the SSB exciter, modulation peaks should read between 180 and 240 ma. The true value of these peaks appreciably exceeds 250 ma. but due to meter inertia and the short duration of peaks, the meter reading is considerably less.

If more convenient, the transmitter may be tuned using the carrier output of the SSB exciter driving the Valiant multiplier and final amplifier. There is then no possibility of forgetting to tune these stages to the correct frequency. The mode switch should be in the SSB position, SW8 Off. Using the carrier control of the exciter and the DRIVE control of the Valiant set grid current near the normal 8 ma. level, turn SW8 On, load the final amplifier to 450 ma. Turn the DRIVE control counter-clockwise to the stop. Switch the exciter to the SSB mode, turn the drive control clockwise until the "buffer" current is 30 ma. Turn up exciter audio gain while talking into the microphone until the meter in the "grid" position barely flicks upward.

10. SSB Tests

SSB performance may be tested using only a cathode ray oscilloscope having an adjustable horizontal sweep and an audio signal generator. The audio signal generator may be a simple oscillator operating at a fixed frequency between 250 and 1000 cycles.

If a SSB transmitter is modulated with a 1000 cycle tone, the output would appear as a continuous wave signal 1000 cycles removed from the original carrier frequency. If the transmitter system for suppressing the carrier is then deliberately upset, an AM sideband will appear at the same frequency but out of phase with the SSB sideband. By adjusting the degree of imbalance in the sideband suppression system and the amount of audio applied thru the exciter audio input jack, an oscilloscope wave form can be produced which appears as a series of positive and negative halves of sine waves, the bottoms of the waves coinciding on a common base line. This scope pattern with rounded tops and bottoms and with intersections forming an "X" are indicative of linear output of the system. The quality of the test pattern obtained from the Valiant departs slightly from the ideal but indicates a degree of linearity far better than required for amateur communication service.

Adjust the final amplifier loading in accordance with the preceding instructions. With the SSB exciter feeding the transmitter in the SSB mode of operation, inject carrier and at the same time introduce the audio signal to the exciter audio input.

Feed a sample of the amplifier output directly to the vertical plates of a cathode ray oscilloscope. Set the internal horizontal sweep to approximately four times the audio modulation frequency. Adjust the amplitude of the RF sample so it fits conveniently in the scope face. Vary the exciter audio control and carrier injection so that the test pattern described is produced. If the halves of sine waves do not meet in the center of the scope, too little audio is being applied. If the tops and bottoms of the wave forms are cut off, too much carrier is being injected. Increase carrier injection and audio to the point where the wave forms are beginning to be slightly distorted by flattening on tops and bottoms. "Plate" current at this point of saturation should be about 300 ma. under conditions of proper loading.

Leave the test set-up as is. Substitute the microphone for the audio oscillator previously used. Readjust the exciter to eliminate the carrier component of its output. Speak into the microphone in a normal manner and adjust the audio control while watching the scope. It will be easy to note the point where peaks start to be clipped. THIS IS THE LIMIT OF AUDIO INPUT. Note the plate current peak reading where clipping just begins with this particular transmitter and do not exceed this current. The indicated peak current will vary depending upon the operator's voice. Peaks of 210 to 240 ma. may be considered typical.

Typical Values - SSB Phone Operation

Amplifier cathode current (resting)	100 ma.
Amplifier grid voltage	-69 volts
Amplifier cathode current (voice peaks)	210-240 ma. (meter reading)
Amplifier cathode current (saturated condition with tone modulation)	300 ma. maximum
Amplifier grid current	Barely perceptible

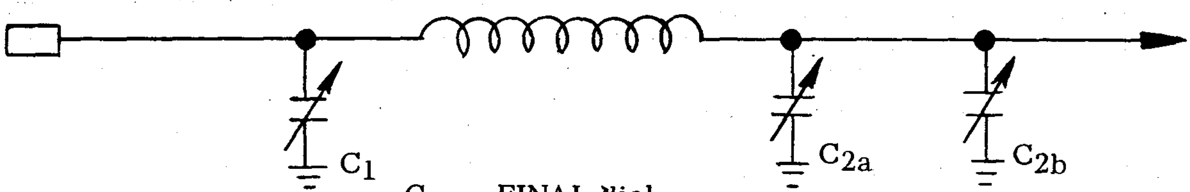
E. PI-NETWORK TUNING AND HARMONIC SUPPRESSION

1. General Information

The pi-tuning/coupling network in the Viking Valiant is designed to load the final amplifier into antenna resistances of nominally 50 to 500 ohms through out the frequency range of the transmitter. In addition, it is capable of "tuning out" series antenna reactances up to several hundred ohms to complete a good match to most unbalanced antenna systems. The range of antenna impedances which may be matched by the pi-network at frequencies higher than 7.0 mcs. extends from roughly 25 to 2000 ohms.

When the transmitter is well grounded and properly tuned, the high harmonic suppression is excellent, generally much better than with other conventional methods of antenna coupling. This should be of interest to amateurs afflicted with TVI or other high frequency interference problems.

The circuit below is the equivalent of the output circuit of the Valiant II.



C_1 - FINAL dial
C_{2a} - AUX COUPLING knob
C_{2b} - COUPLING FINE knob

The tuning technique consists of resonating the circuit initially with C_1. Both C_{2a} and C_{2b} are at their counter-clockwise (maximum capacity) positions. The amplifier is coupled to the load by successively reducing the capacity of C_{2a} and/or C_{2b} in small increments and tuning out reactance after each capacity change by tuning C_1 to resonance (minimum current). As the antenna takes power, the minimum amplifier current is established at progressively higher levels until the amplifier is loaded to full rated power input.

2. Importance of Grounding

To obtain proper tuning, coupling and harmonic suppression with any unbalanced transmitter antenna coupling system, the part of the circuit designed to operate at RF ground potential must be at RF ground potential. A "room full of RF" is evidence that a high RF potential exists on some object in or near the room. In many cases the source of RF appears to be the transmitter chassis and power cord. This condition is very undesirable for several reasons. The power cord is very closely coupled to the chassis by the electrostatic shields of power transformers. Three objectionable factors affecting transmitter performance when poor grounds are involved are:

a. The impedance that the output terminal of the transmitter looks into includes not only the true antenna to ground impedance presented by the feed line but also the equivalent series transmitter chassis to ground impedance. This additional impedance can, in some cases, raise the apparent antenna impedance to such a high value that it cannot be loaded by the pi-network.

b. Part of the transmitter power is lost in the ground system due to radiation of the ground lead, power cord or cabinet. This power is quickly dissipated in surrounding objects and contributes nothing to effective radiated power.

c. Practical design considerations make it necessary to bypass possible sources of stray high frequency currents to the transmitter chassis. When a high impedance exists between transmitter chassis and ground these stray currents can radiate to a certain extent.

3. How to Obtain a Good Ground

What may appear to be a good ground at one frequency may prove to be a poor ground at another. A single ground lead may have "standing waves" on it due to its length. While it may seem difficult to obtain a good ground over a wide range of frequencies, it can be done and will be well worth the trouble when increased radiation efficiency, ease of antenna loading and reduced TVI and BCI result. There is also reduced danger of damaging microphones, receivers and other associated equipment with excessive RF fields.

Avoid using the power line, power line conduit or gas lines for RF grounding. Some suggestions which may help to obtain a good ground are:

a. Water pipes or metal building structural members are usually good sources of earth grounds.

b. Use heavy conductors (#14 or larger) between the connection at the ground point and the transmitter. Copper ribbon is excellent for this purpose.

c. The use of several ground leads, each of a different length and selected at random may be helpful in keeping the grounding impedance low at the transmitter, even though the transmitter is some distance from a true earth ground. The possibility of obtaining an effective ground at any frequency throughout the transmitter's range is quite good. If at any one frequency, one of the ground leads presents a low impedance at the chassis, the chassis is effectively grounded. By changing the length of one of the ground leads experimentally, a good ground can often be obtained at a frequency which has been troublesome. In bringing several leads to the transmitter, small closed loops near the transmitter or antenna feed line should be avoided. Induction fields will tend to raise the impedance of the ground leads.

d. In cases where it is impossible to obtain a good earth ground, connecting the transmitter chassis to some system of conductors having a very low effective impedance to ground compared to the antenna impedance may be helpful. Usually this artificial "ground" takes the form of a system of radial wires spread horizontally on the floor, a gridwork of wires, or a large metal sheet on the floor below the transmitter. To be most effective, the minimum area covered by the metal conductors should be roughly equivalent to a square, the length of one side of which approaches a quarter wavelength at the lowest operating frequency. This system of grounding should be experimented with before committing the location to any permanent installation.

e. A simple counterpoise made up of a single wire attached to the chassis may be helpful. On 10 meters, a length of 6 to 8 feet may be attached and the open end cut off 4 inches at a time until the chassis becomes "cold". The open end of the wire may be allowed to drop along the floor although its open end will be somewhat "hot" with RF.

f. A rough check on the effectiveness of the transmitter ground may be made by touching the chassis while watching the PA plate current and grid current with the transmitter operating into an antenna. A change in current upon touching the chassis is indicative of an ineffective ground. In cases where the transmitter is feeding a low impedance antenna, test by touching the cabinet with a neon lamp. The presence of 50 to 60 volts will ignite the neon lamp.

4. Loading Random Antennas

With the transmitter chassis well grounded, correctly designed antenna systems having relatively "flat" unbalanced feeder systems can easily be loaded by following the instructions previously given. This assumes that the antenna terminal impedances fall within the range of the pi-network. If the feedline is over a quarter wavelength long, feeding a balanced system (one transmission lead to the center terminal of J6, the other side to transmitter ground stud) may prove surprisingly successful provided the transmitter cabinet is held at ground potential. Some standing waves will result but may not prove excessive. The Johnson Matchbox, a universal all band, bandswitch antenna coupler will permit loading of the Viking Valiant II to any practical antenna system. In addition, it provides for the use of the Johnson 250-20 Low Pass Filter for increased harmonic suppression.

Antennas having random length, random feed points and various types of feed lines will exhibit widely different resistance and reactance characteristics. It is well to remember that the feedline is a very important part of the system. A common example of the random antenna is a horizontal wire fed by a single wire feed line. The feed line in this case actually becomes part of the radiating system. An antenna of this type can, in most instances, be fed by the pi-network directly but there are critical dimensions where the antenna series reactance (inductive or capacitive) becomes too high and the antenna resistance can become either too high or too low to be matched by the pi-network.

Antennas with high terminal resistance or reactance can be recognized while loading the output stage of the Viking Valiant II. The final amplifier is loaded by reducing the total of the output coupling capacity by adjusting either or both the AUX COUPLING and FINE COUPLING controls. As the output coupling capacity is reduced in small steps, retuning the amplifier to resonance each time, the minimum plate current is increased. Normally this process is continued until full loading of the amplifier is achieved. If, however, a point is reached where decreasing the output coupling capacity does not result in a marked increase in PA plate current and the PA is not fully loaded, the antenna can be assumed to have a high resistance or reactance at this frequency.

Antennas with low terminal impedance (resistance and reactance both low) can be recognized by a noticeable lack of coupling capacitor effect in the range of settings normally used at the operating frequency. It may prove impossible to decouple the amplifier sufficiently for normal loading.

Several methods may be used in an effort to bring the antenna system into the tuning range of the pi-network.

a. Change the length of the feeder line between the antenna and transmitter experimentally 1/8 to 1/4 wavelength.

b. Change the point of connection of the feedline to the antenna 1/8 to 1/4 wavelength.

c. Change the antenna length 1/8 to 1/4 wavelength. Antennas shorter than 1/8 wavelength (antenna and feeder) may be difficult to load. They present a high capacitive reactance to the transmitter output terminals. Effective antenna length in the vicinity of 1/2 wavelength will have little reactance but very high resistance making them difficult to load.

d. "Load" the antenna feeder by placing an inductor or capacitor in series to cancel out the reactance of the antenna feeder. This may require considerable cut and try and will affect only the reactive component of the antenna impedance. It does prove useful in some cases.

e. L type matching networks of inductance and capacitance may be used to aid impedance matching. Much discussion of this more elaborate method of bringing the antenna impedance within the range of the pi-network could be included, however, the few cases where it is necessary do not justify inclusion herein. Textbook and handbook discussions will be helpful if work along this line is pursued. There is danger of resonating the coupling capacitor of the pi-network when using an external coil. This should be watched as excessive voltage built up across the coupling capacitors can cause damage. Improper coupling or loading will take place under these conditions.

5. Loading Precautions

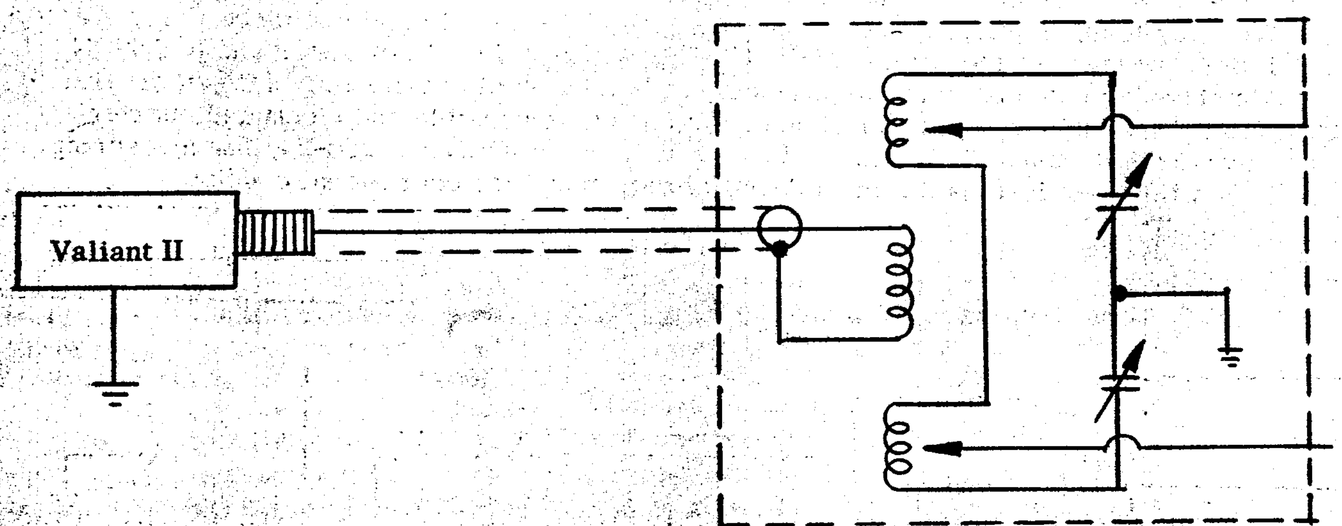
When loading high impedance antennas there is a temptation to "squeeze" the last watt into the antenna by opening the coupling capacitors as much as possible. Harmonic suppression is dependent, to a great extent, on the amount of coupling capacity remaining in the circuit. <u>It is wise to use as much coupling capacity as is practical at all times.</u>

The proper amount of coupling when antenna impedance is high, can be conveniently determined by holding a neon lamp against the antenna feeder. The coupling capacitor can then be opened until little increase in glow is noticed when the coupling capacitor and tuning controls are adjusted for maximum output. A decrease in coupling capacitance beyond this point may cause a higher plate current reading due to reduced plate circuit efficiency. Higher harmonic output will also result as the coupling capacity is reduced beyond the point where output has levelled off. The random antenna system may present a more favorable impedance to harmonic output than the output on the fundamental frequency; hence it is well to use as much coupling capacity as is practical. It is well to remember that the amount of coupling capacitance needed is dependent on operating frequency. For example, 2,000 micro microfarads at 3.5 mcs. corresponds to 160 micro microfarads at 28.0 mcs. These are the values necessary to couple resistive loads of approximately 50 ohms, at the frequencies stated.

If the power line voltage is low or the high voltage rectifiers have low emission, the loaded plate current may not reach the normal value. This condition should not be confused with the inability of the pi-network to load an antenna system.

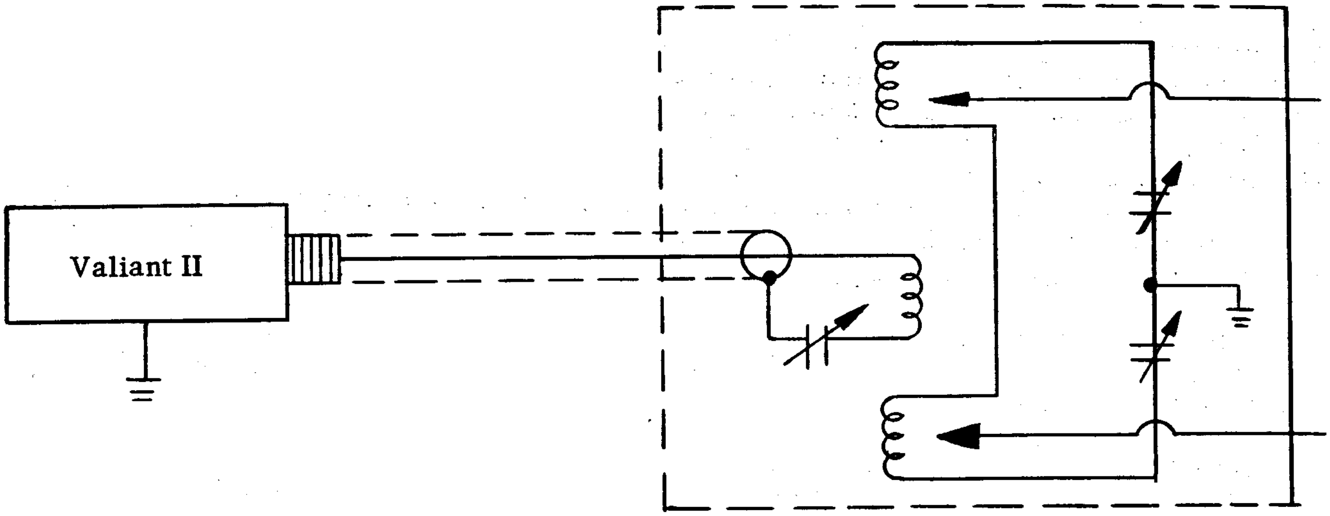
6. Coupling to Balanced Loads

Balanced antennas such as center fed "Zepps", beams and folded dipoles normally use a two wire transmission line and should have equal voltages, 180 degrees out of phase, applied to each feedline terminal. Since the output of the Viking Valiant II is single ended, unbalanced, a coupler is required for balanced antenna systems. The JOHNSON Matchbox, a universal, all band, bandswitched antenna coupler will permit loading of the Valiant II to any practical antenna system. In addition, it provides for the use of the JOHNSON 250-20 Low Pass Filter for increased harmonic suppression. A simple coupler for this purpose is shown below. The tank circuit is resonant at the operating frequency and can be excited by a coaxial line and coupling link. Line impedance is not critical although 52 ohms line will be most desirable if a JOHNSON Low Pass Filter is used.



Feedpoint impedance of the coupler is adjusted by means of the inductor taps. Tap adjustment is unnecessary with the JOHNSON Matchbox. Final amplifier loading is adjusted with the transmitter output coupling controls.

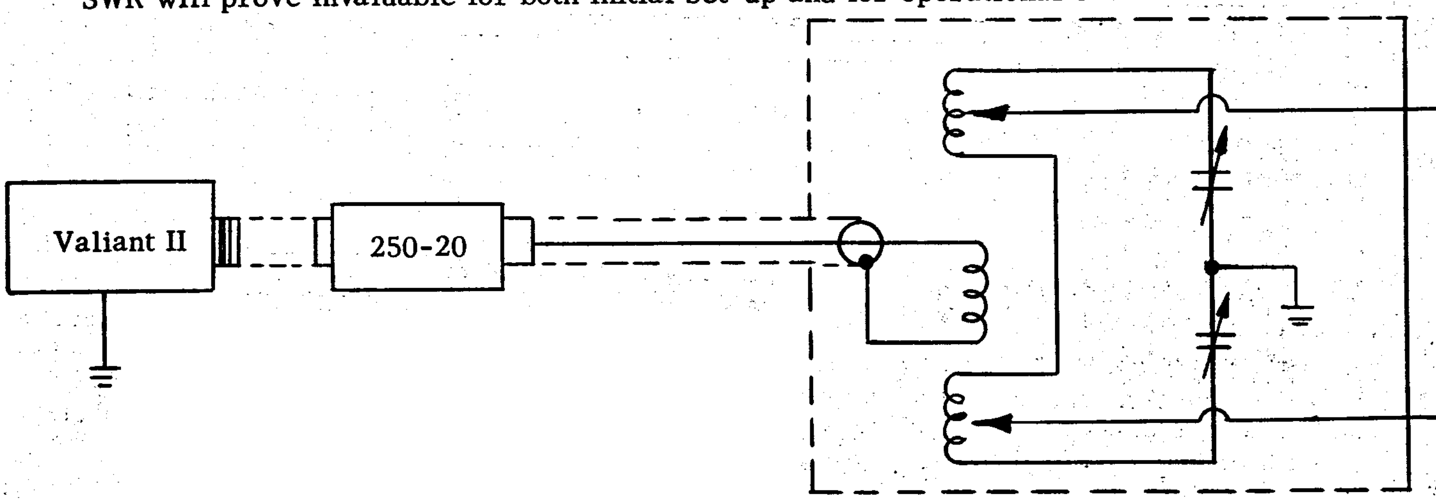
Tuning of the coupler can be made quite broad by making the L/C ratio as high as possible (low Q) while still permitting the desired loading. Inductive reactance of the coupling link may make it impossible to reduce the SWR of the coaxial line to below 1 1/2 to 1. If so, the link circuit may be made series resonant by adding capacitor C_1 as shown on adjacent page.



This problem is non-existant with the Matchbox.

7. Use of Low Pass Filters

Depending upon how it is tuned, 2nd harmonic attenuation of the Viking Valiant II amplifier can be as high as 30 db. Since this will permit operation in many locations without television interference, the JOHNSON 250-20 Low Pass Filter is not an integral component of the Valiant II, but is available as an optional accessory. This filter will provide an additional 75 db or more harmonic attenuation with insertion loss less than .25 db. Characteristic impedance is 52 ohms, power rating 1 KW. The low pass filter may be inserted in the coaxial line between the transmitter and the antenna coupler. Coaxial connectors are used at the transmitter and at both ends of the low pass filter to preserve the shielding provided by the coaxial line. It is preferable that the standing wave ratio on the coaxial line between the Valiant II and the coupler be maintained at 2 to 1 or less, therefore, the impedance of the line should be the same as the characteristic impedance of the filter. (THE JOHNSON 250-20 Low Pass Filter and JOHNSON Matchbox are both 52 ohms impedance.) The section of coaxial line between the transmitter and the low pass filter should be as short as possible and electrical quarter waves should be avoided. An RF bridge such as the JOHNSON 250-24, for measuring SWR will prove invaluable for both initial set-up and for operational checks.



An end fed half-wave antenna may present loading problems, both from the standpoint that its impedance is higher than can be matched by the pi-network amplifier of the Valiant II, or that the low output coupling capacitance used reduces inherent harmonic attenuation below tolerable values. Therefore, the use of a half wave antenna may create TVI problems while other antennas prove perfectly satisfactory. In these cases it is recommended that the JOHNSON Matchbox be used.

F. VFO CALIBRATION

1. Definitions and General Information

The following instructions are for calibrating the Viking Valiant II VFO using a signal generator for the frequency standard and a receiver capable of tuning the calibration frequencies.

The accuracy of the Valiant II VFO calibration will be no better than that of the signal generator used to calibrate it. To fully utilize the stability and calibration capabilities of the VFO, the frequency standard used to calibrate it should have an accuracy of .005% or better. Most crystal standards or crystal calibrated variable frequency standards are satisfactory for normal calibration purposes. A moderate signal output is required, capable of being easily detected with the receiver to be used for zero beat indication.

The frequencies F1a, F2a, F3a and F4a used in the text following are indicated output frequencies of the calibrating standard. The abbreviations F1, F2, F3 and F4 are VFO dial settings corresponding to frequencies F1a, F2a, F3a and F4a respectively. (F1a, F2a, F3a and F4a may be either fundamental frequencies or any harmonic it is desired to use.)

F1a Any given frequency (preferably a frequency corresponding to a low frequency VFO dial calibration mark) between 1.75 and 1.78 mcs. or any of the first eight harmonics of 1.75 to 1.78 mcs. in the range of the receiver. 1.76, 3.52, 5.28, 7.04 and 8.80 mcs. are good calibrating frequencies.

F2a Any given frequency (preferably a frequency corresponding to a low frequency VFO dial calibration mark) between 1.96 and 2.00 mcs. or any of the first eight harmonics of 1.96 to 2.00 mcs. in the range of the receiver. 1.97, 3.94, 5.91, 7.88 and 9.85 mcs. are good calibrating frequencies.

F3a Any given frequency (preferably a frequency corresponding to a high frequency VFO dial calibration mark) between 7.00 and 7.07 mcs. or any of the first four harmonics of 7.00 to 7.07 mcs. in the range of the receiver. 7.03, 14.06, 21.09 and 28.12 are good calibrating frequencies.

F4a Any given frequency (preferably a frequency corresponding to a high frequency VFO dial calibration mark) between 7.35 and 7.425 mcs. or the first four harmonics of 7.35 to 7.425 mcs. 7.40, 14.800, 22.2 and 29.6 mcs. are good calibrating frequencies.

Warm up the signal generator for at least half an hour or as long as suggested by the signal generator instructions before using it for VFO calibration.

Set up a receiver capable of detecting each of the frequencies selected. Attach antenna leads to the receiver input and the signal generator output. (Three or four foot lengths will probably be ample.) Bring the leads closer together until signal generator output can be picked up by the receiver. Separate and shorten the leads as found necessary to keep the receiver from blocking due to excessive signal input. Allow the receiver to warm up for about 1/2 hour to stabilize the local oscillator and log dial settings for frequencies F1a, F2a, F3a and F4a. The beat frequency oscillator in the receiver may be used to log and compare the signal generator and VFO frequencies but it is desirable to obtain the final zero beat indications between VFO and signal generator signals without the beat frequency oscillator. Avoid setting the receiver on or logging image frequencies.

Warm up the Viking Valiant II in the "zero" position of the OSCILLATOR switch with SW8 off for 1/2 hour. Turn the bandswitch to the 160 or 80 position. Turn the VFO dial pointer to the frequency F1, between 1.75 and 1.78 mcs. chosen for the low 160 meter calibrating point and find it or its harmonic (near F1a) on the receiver. Repeat the same procedure at the high 160 meter calibrating point and the 40 meter high and low points after moving the bandswitch to the 40 meter position.

2. 160, 80 Meter Scale Calibration

Set the Valiant bandswitch on the 160 or 80 meter position and the dial at F2, the dial reading corresponding to the frequency between 1.96 and 2.00 mcs. chosen for the high 160 meter calibrating point. Set the signal generator to F2a and tune in the signal on the receiver. Adjust the "160 hi" trimmer on top of the VFO (Figure 1) until the VFO zero beats with the signal generator.

Turn the signal generator to F1a, tune the receiver to the same frequency, turn the VFO to F1 and adjust the "160 lo" padder atop the VFO until the VFO zero beats with the signal generator.

Repeat the "160 hi" and "160 lo" adjustments, zero beating the signal generator and VFO as accurately as possible. Since the adjustments affect each other several repeats of the adjustments may be necessary before attaining the most accurate setting possible.

3. 40, 20, 15, 10 Meter Scale Calibration

Set the Valiant II bandswitch on the 40 or 20 meter position and the dial pointer at F4 on the high frequency dial scale, the frequency between 7.35 and 7.425 mcs. chosen for the high 40 meter calibration. Set the signal generator and the receiver at F4a. Adjust the "40 hi" trimmer at the top of the VFO until the VFO zero beats with the signal generator.

Turn the VFO to F3, the setting corresponding with the frequency between 7.00 and 7.07 mcs. chosen for the low 40 meter calibration, the receiver to F3a, the signal generator to F3a and adjust the "40 lo" padder until the VFO zero beats with the signal generator.

Repeat the "40 hi" and "40 lo" adjustments, zero beating the signal generator and VFO as accurately as possible.

4. 11 Meter Calibration

The 11 meter band VFO output is near 6.75 mcs. A given frequency, F5a, in the range 6.7 to 6.85 mcs. or any of the first four harmonics of the 6.7 to 6.85 mcs. range may be used to calibrate the 11 meter range. Turn the Valiant II bandswitch to the 11 meter band, set the VFO dial to the position F5 corresponding to the frequency F5a or its harmonic which falls in the 11 meter band. Set the receiver to the 11 meter range or a subharmonic and detect the standard signal frequency. Adjust the "11 meter" trimmer until the VFO zero beats with the standard frequency.

Recheck the 40 to 20 meter calibration after the 11 meter adjustment. There is little likelihood that further readjustments are necessary unless a large change was required in the "11 meter" setting.

5. Calibration Against Crystals

Crystals of known frequency and accuracy in the frequency ranges F1a, F2a, F3a, F4a (designated in section F1) may be used in the transmitter crystal oscillator to provide standard frequency signals for the VFO calibration. The stability of the receiver local oscillator and beat frequency oscillator must be nominally good as the technique of beating the receiver BFO to the crystal and then beating the VFO signal to the receiver will be used. The receiver thus "remembers" the crystal frequency. Reduce the coupling of the receiver antenna to the minimum useable amount to avoid "pulling" of the local oscillator.

An example of calibrating the VFO using actual crystal values may be helpful. Assum that the following crystals have been found as part of the amateur station equipment: 7060 kcs., 3690 kcs. and 1980 kcs. The dial calibration points then become:

$$F1 = \frac{7.060}{4} = 1.765 \text{ mcs.}$$

$$F2 = 1.980 \times 1 = 1.980 \text{ mcs.}$$

$$F3 = 7.060 \times 1 = 7.060 \text{ mcs.}$$

$$F4 = 3.690 \times 2 = 7.380 \text{ mcs.}$$

The receiver setting and VFO harmonic which may be used for each respective dial calibration frequency then becomes:

$$F1a = 7.060 \times 1 = 7.060 \text{ mcs.}$$

$$F2a = 1.980 \times 4 = 7.920 \text{ mcs.}$$

$$F3a = 7.060 \times 1 = 7.060 \text{ mcs.}$$

$$F4a = 3.690 \times 2 = 7.380 \text{ mcs.}$$

Proceed as follows:

a. Place the 1.980 mc. crystal in the C1 position of J7 (pins 3 and 5) and the 7.070 mc. crystal in the C2 position (pins 7 and 1 of J7).

b. Set the bandswitch on 160 or 80 meters, the VFO dial pointer on the 1.980 mc. mark, the OSCILLATOR switch on C1 position. (Leave SW8 off throughout calibration). Tune the receiver to zero beat the BFO with the crystal. Turn the OSCILLATOR switch to the VFO position and adjust the "160 hi" trimmer to zero beat the receiver BFO.

c. Set the VFO pointer on the 1.765 mc. mark, the OSCILLATOR switch to the 7.060 mc. position (C2). Tune the receiver to zero beat the BFO with the crystal. Turn the OSCILLATOR switch to VFO and adjust the "160 lo" padder to zero beat the BFO. Repeat steps b and c as necessary to cancel out interaction between the "160 lo" and "160 hi" adjustments.

d. Remove the 1.980 mc. crystal from the C1 position and replace it with the 3.690 mc. crystal.

e. Set the bandswitch on 40 meters, the VFO dial pointer to 7.380 mcs. and the OSCILLATOR switch to C1. Tune the receiver to zero beat the BFO with the crystal. Turn the OSCILLATOR switch to VFO and adjust the "40 hi" trimmer to zero beat the BFO.

f. Set the VFO pointer on 7.060 mcs. and the OSCILLATOR switch to C2. Tune the receiver to zero beat the BFO with the crystal. Turn the OSCILLATOR switch to VFO and adjust the "40 lo" padder to zero beat the BFO. Repeat steps e and f to minimize adjustment reaction.

g. The 11 meter band setting may be made with a crystal which will place a harmonic signal in the 11 meter band. Set the bandswitch on 11 meters, the OSCILLATOR switch to the crystal (assume 1.810 mcs. is available) position. Zero beat the receiver BFO to 27.150 mcs. (the 15th harmonic of 1.810 mcs.) Turn the OSCILLATOR switch to VFO and adjust the "11 meter" trimmer to zero beat the VFO to the receiver BFO.

h. Recheck the "40 hi" and "40 lo" adjustments, steps e and f.

The user may think of several sources of standard signals other than those mentioned. In each case the accuracy of the source should be known before using it. Many combinations of harmonics can be found and no attempt has been made to cover all of them in this discussion. Other signal sources which may be used but are not covered here are:

a. The signal of another amateur station whose frequency has been determined by a standard.

b. The harmonics of a signal generator the output signal of which has been zero beat with a broadcast station.

c. Signals of WWV discussed in the next topic.

The user must adapt his techniques to the signal source he has available.

Band edge crystals or crystals near the usual operating frequencies of the amateur station are always valuable for occasional monitoring of the VFO signals. They may be used in a separate oscillator circuit or the crystal oscillator stage of the transmitter.

6. Calibration Against WWV

The following technique for calibration against the WWV 10 mc. signal is not recommended if other standard signal sources are available. It will be noted that most calibration points are on the ends of the bands. While the 160 or 80 meter calibration is accurate the 40, 20, 15 and 10 meter calibration includes the tracking error of the VFO low frequency band (160, 80). The receiver, the receiver BFO and VFO should be warmed up 1/2 hour before calibrating.

a. Zero beat the receiver BFO with the 10 mc. WWV signal.

b. Set the VFO dial pointer to 2.00 mcs., the bandswitch on 160 meters.

c. Adjust the "160 hi" VFO trimmer until the fifth harmonic of the VFO is zero beat with the receiver BFO.

d. Leaving the VFO at this setting, zero beat the receiver BFO with the seventh harmonic of the VFO (14 mcs.)

e. Turn the VFO to 1.75 mcs. and adjust the "160 lo" VFO padder to zero beat the eighth harmonic of the VFO with the receiver BFO.

f. Adjust both ends of the 160 meter band to zero beat the eighth and seventh harmonics of the VFO with the receiver BFO as necessary to cancel adjustment interaction.

40, 20, 15 and 10 Meter Calibration

g. Set the VFO dial at the 1.85 mc. mark and zero beat the receiver BFO to the eighth harmonic of the VFO frequency at 14.8 mcs.

h. Set the bandswitch to 40 meters and the dial pointer to the 7.40, 29.6 mc. mark. Zero beat the second harmonic of the VFO to the 14.8 mcs. receiver setting by adjusting the "40 hi" trimmer.

i. Set the bandswitch and dial pointer for 1.75 mc. VFO output again and zero beat the receiver BFO at 14 mcs. Set the bandswitch and dial for 7.0 mc. VFO output. Adjust the "40 lo" padder to zero beat the VFO second harmonic with the receiver 14.0 mc. BFO setting.

11 Meter Calibration

j. Set the bandswitch and VFO dial for 1.80 mc. output.

k. Tune the receiver to 27 mcs. and zero beat the receiver BFO to the fifteenth harmonic of the VFO.

l. Set the bandswitch on 11 and the dial pointer on 27.0 mcs. Adjust the "11 meter" trimmer to zero beat the fourth harmonic of the VFO to the receiver BFO setting.

7. Calibration Trouble Shooting

If the VFO frequency cannot be adjusted to the dial markings due to apparent lack of trimmer or padder range.

Check to make certain the frequency standard used is accurate (crystals used in amateur service are often found to differ from their marked frequency due to holder conditions, oscillator circuit loading or non-critical original calibration).

Make certain image frequencies are not being mistaken for desired frequencies in the receiver.

If, after checking the frequency standard and receiver settings, the VFO frequency cannot be adjusted to chosen dial marks, adjust the trimmers to bring the VFO as close as possible to correct calibration. Remove the VFO slide cover and recheck the dial location relative to the tuning capacitor shaft. The VFO tuning capacitor should be exactly meshed (not necessarily the stop position) when the dial pointer is precisely horizontal to the left. If the dial pointer requires re-positioning, loosen the two set screws in the shaft coupler attached to C1 from beneath the chassis, re-set the dial, tighten both set screws. This should permit the VFO to be calibrated properly.

8. VFO Temperature Compensation.

Capacitor C116 was adjusted at the factory for the proper temperature compensation. If for some reason C116 has been inadvertently tampered with or the temperature compensation appears not to be satisfactory, the following procedure should be used to readjust the temperature compensation.

CAUTION: The signal source used to compare the Valiant II VFO must be very stable. A 100KC crystal calibrator is suitable. Do not rely on a receiver's frequency stability, as many receivers drift more than this VFO. The receiver will be used only as a mixer and as such will not affect the accuracy of the measurements. Warm up all equipment a minimum of one hour.

Procedure:

a. Warm up the receiver, crystal calibrator and Valiant II for a minimum of one hour.

b. Tune the receiver to 7.3 megacycles by turning on the receiver BFO and zero beating the receiver against the 100KC crystal calibrator and then turning off the BFO.

c. After the prescribed warmup period, switch the Valiant II to 40 meters and tune to 7.3 megacycles. Listen for the beat against the 100KC crystal oscillator in the receiver. Adjust the VFO dial for exact zero beat.

d. Allow about 10 minutes (or longer if necessary) until an audible signal is heard in the receiver. Carefully return the VFO dial to zero beat the signal being very careful to note the direction required to do this.

e. If the VFO signal was lowered in frequency to re-zero, turn C116 slightly clockwise (less negative temperature coefficient), then readjust the 40 meter high trimmer to reset the frequency if necessary.

f. If the VFO signal was raised in frequency to re-zero, turn C116 slightly counter-clockwise (more negative temperature coefficient), then readjust the 40 meter high trimmer to reset the frequency if necessary.

g. Repeat steps 4, 5, and 6 as necessary.

h. Finally cool the Valiant II off and repeat the frequency stability check to determine how much improvement has been made.

i. Typical stability after a 30 minute warm-up is approximately .001% or less per hour. On any temperature compensated device a slight drift above or below the "final" frequency can be expected over long time periods due to cycling of the compensating components. Since this is a slow process, it can be considered negligible.

G. TROUBLE SHOOTING

1. Operational problems may be due either to tube failure, component failure or improper operational technique.

Frequently, malfunction of a piece of equipment such as the Valiant II is the result of a tube failure. Meter readings will usually indicate the probable stage affected and servicing requires only substitution of known good tubes. In any case, tubes should be tested first and eliminated as the source of trouble.

As a rule, a component failure in a piece of equipment such as the Viking Valiant II will produce more than one abnormal value of current or voltage or both. The effect of a component failure will usually be noticed on more than one meter reading and in more than one stage of the transmitter. Portions of each circuit are almost invariably common to another circuit and this factor should be noted for analyzing troubles for speedy systematic servicing.

For example, suppose that the meter M1 in the "oscillator" position reads almost zero current. "Buffer" current reading is low but probably due to the fact that the buffer is receiving no excitation. There is no grid current to the final amplifier but this is to be expected since the crystal/buffer stage (V3) appears not to be functioning. Listening carefully on the receiver reveals that the VFO is oscillating. Under these conditions, the common factor would appear to be the source of plate or screen voltage for either V1 or V3. Since the socket XV1 is not readily accessible and since there must be voltage at each end of R5, (it was determined V1 is oscillating) then it would be wise to assume that the VFO is normal until all the easier checks have been made. A voltage check at pin 3 or 8 of V3 shows the screen voltage to be zero. A check of components would reveal that R8 (68K ohms) is burned out, caused by V3 being shorted, C27 shorted or an accidental ground of pin 3 or 8 of socket XV3.

To service the equipment make liberal use of current values, normal voltage readings and resistance measurements appearing in this manual. Use these values in the order stated. Abnormal dial readings may be used to analyze difficulties in RF circuits. Make the easy checks first, look first for simple faults but remember that a component failure often produces a second collateral component failure and to restore normal operation both must be remedied.

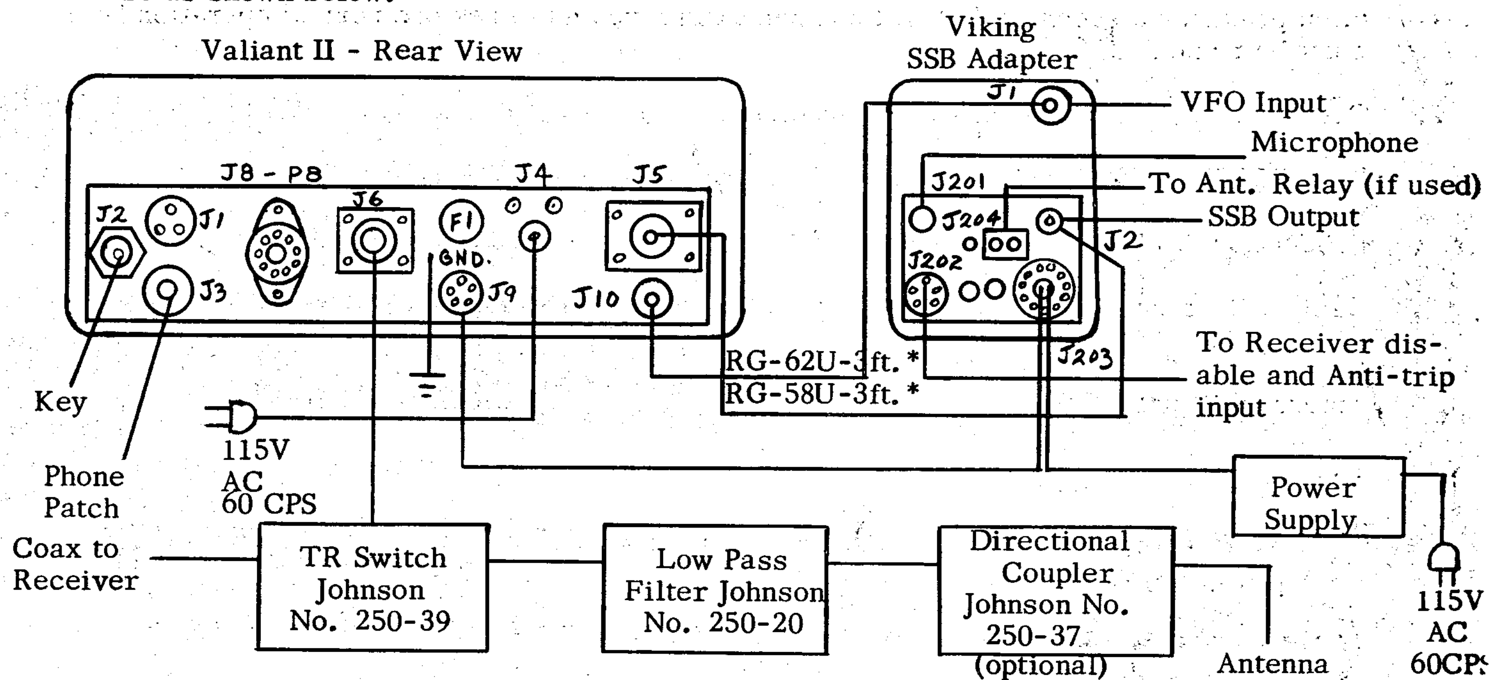
2. Operating Problems and Possible Remedies:

"Zero" OSCILLATOR switch position blocks receiver	- - SW8 in "man" position
RF Section dead	- - P8 disconnected
Hum on Carrier	- - Defective preamplifier tubes microphone shield not grounded.
Antenna will not load	- - Review section E5
TVI	- - Review section E7
Poor Audio quality	- - CLIPPING control in extreme CCW position (max clipping)
VFO unstable	- - Marginal setting of keying pot R39
Crystal Oscillator inoperative	- - Crystals plugged into wrong socket pins, C1, pins 3 & 5 of J7, C2 pins 7 & 1 of J7
Modulator tubes run red	- - Check bias adjustment, check for RF on cabinet causing feedback
Modulator current swing too low	- - Excessive bias defective audio or modulator tube RF feedback saturating modulator
Reverse grid current	- - Excessive drive to final amplifier tubes
Low final amplifier plate current	- - Clamper adjusted incorrectly. Incorrect bias adjustment. Mode switch on SSB Low grid drive one or more 6146s not lighting.

H. INTER-UNIT CABLES FOR SSB OPERATION

1. Valiant II to Viking SSB Adapter

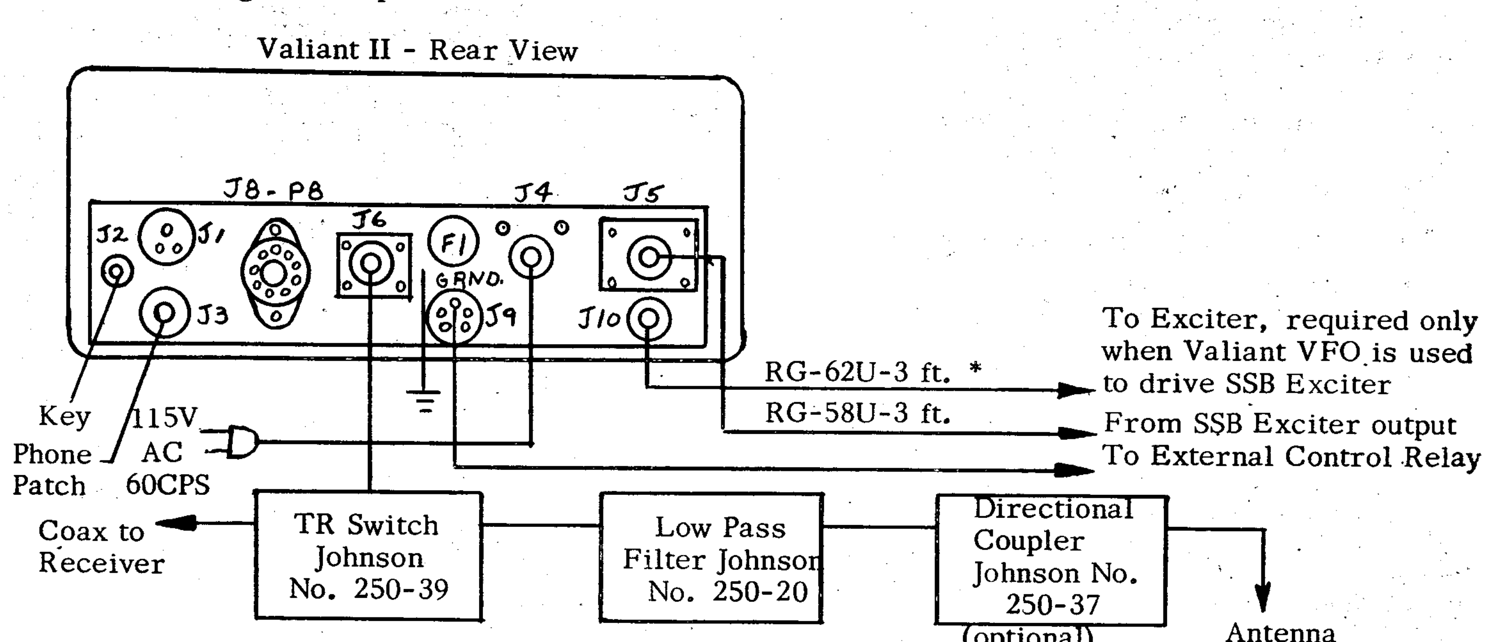
The cable requirements for connecting the Valiant II to the Viking SSB Adapter are as shown below.



* The RG-62/U and RG-58/U cables must be made exactly 3 feet long

2. Valiant II to SSB Exciter

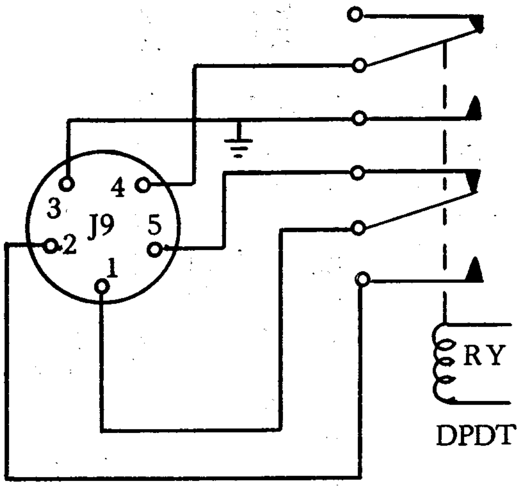
The cable requirements for connecting the Valiant II to a SSB Exciter other than the Viking SSB Adapter are shown below.



* The RG 62/U should be made exactly 3 feet long.

3. External Relay Connection to Valiant II

Connection of an external relay to the Valiant II J9 jack for SSB exciters other than the Viking SSB Adapter.



Standby

Operate

Pin 1 of J9 connects to 6146 grids
Pin 2 of J9 - operating bias
Pin 3 of J9 connects to ground
Pin 4 of J9 connect to relay if Valiant VFO is used
Pin 5 of J9 - blocking bias

DPDT External Relay
This relay and connecting cable are furnished with the Viking SSB Adapter.

I. VALIANT II AS AN EXCITER

The Valiant II may be used as an exciter for a high power amplifier when a modification is made in its circuit. When modified, the Valiant II will furnish R.F. drive to the final amplifier and audio drive to the high power modulators.

When the Valiant II is used as an exciter, the lead from terminal 1 of SW4B (see Figure 9) must be opened to prevent +600 volts being applied to the grid of the modulators when the MODE switch is in the CW and SSB positions. When operating the Valiant II by itself, the open lead from terminal 1 of SW4B must be closed for proper operation of the unit.

Operation of the Valiant II as an exciter will require a new plug to be inserted in J8 (see Figures 9 and 12C). The plug's terminals 5 and 6 should be jumpered together and terminals 7 and 8 should also be jumpered together. A shielded wire supplying the bias voltage to the grids of the high power modulators should be connected to terminal 1 of the plug. A shielded lead from the grid of one of the modulators should be connected to terminal 2 of the plug. Another shielded lead from the other modulator grid should be connected to terminal 3 of the plug. Connect all lead shields to terminal 9 of the plug and also to a ground near the modulator tubes.

A 1000 ohm 10 watt resistor should be connected from the grid of each high power modulator to the lead supplying the modulator bias voltage. These resistors will improve the regulation of the driver and dissipate some of the excessive audio power. A .005 mfd capacitor connected from ground to each of the modulator grids and to the lead supplying the modulator bias voltage will bypass any possible RF in the circuit to ground.

TABLE 1
VIKING VALIANT II TRANSMITTER SOCKET VOLTAGES

Line Voltage	117V	Final Plate	330 ma.
Mode - AM Phone	(no audio signal)	Final Grid	8.0 ma.
RF Load	50 ohm	RF Output Freq.	7.0 mcs.
Clipping Control at	10	H.V.D.C.	630V Mod.

H.V.D.C. 620V Final Amp (Measure at term. 3 of TS18)

Tube Socket		1	2	3	4	5	6	7	8	9
		Tube Socket Pin Number								
XV1	6AU6				(See note 1)					
XV2	OA2				(See note 1)					
XV3	6CL6	0	NC	145	5.7AC	-	330	-	NC	-6
XV4	5763	330	13	-	5.9AC	-	(50-170)	13	-11	NC
XV5	6146	-	5.95AC	180	-	-69*	-	-	-	
XV6	6146	-	5.95AC	180	-	-69*	-	-	-	
XV7	6146	-	5.95AC	180	-	-69*	-	-	-	
XV8	6AQ5	NC	0	-	5.95AC	146	146	-6.5		
XV9	OC3-VR105	NC	0	100	NC	106	NC	108	NC	
XV10	OC3-VR105	NC	105	100	NC	217	NC	108	NC	
XV11	12AU7	-.65	-150	12	-	-	330	0	12	5.8AC
XV12	12AX7	95	-.5	-	-	-	182	0	1.2	6.0AC
XV13	6AL5	85	85	-	6.0AC	85	330	85		
XV14	6C4	160	NC	-	6.0AC	160	0	7.5		
XV15	12AU7	330	0	14	-	-	330	0	14	6.0AC
XV16	6146	0	6.2AC	218	NC	-46	NC	-	NC	
XV17	6146	0	6.2AC	218	NC	-46	NC	-	NC	
XV18	866	675	625	330	675					
XV19	866	675	NC	0	675	NC				
XV20	5V4	NC	370	340	305AC		305AC	NC	370	
XV21	6BY5GA	210AC	6.2AC	NC	-262	-262	-235	0	210AC	

a - Measure at junction of L7 and R57
\- Ground to Chassis
* Adjust for 100 ma. idling P.A. current when mode switch is in SSB position under local line voltage conditions.
NC No Connection
Note 1: Because XV1 and XV2 are not readily accessible, voltages are listed for terminal strip TS6 underneath the VFO.

Terminal	Voltages	Terminal	Voltages
1	-.65	5	5.8AC Measured with 20K ohms/V meter
2	5.8AC	6	340
3	.05	7	.05
4	0	8	0

Voltage tolerance, plus or minus 20%

TABLE 2
VIKING VALIANT TRANSMITTER RESISTANCE MEASUREMENTS*

Tube Socket		Tube Socket Pin Number 1	2	3	4	5	6	7	8	9
XV1	6AU6				(See note 1)					
XV2	OA2				(See note 1)					
XV3	6CL6	0	NC	80K	.05	-	12.5K	-	NC	100K
XV4	5763	12K	450	-	.05	-	a.0-12.5K	500	70K	NC
XV5	6146	-	.05	50K	-	b.0 to 4K	-	-	-	
XV6	6146	-	.05	50K	-	b.0 to 4K	-	-	-	
XV7	6146	-	.05	50K	-	b.0 to 4K	-	-	-	
XV8	6AQ5	NC	.3	-	.05	50K	50K	200K		
XV9	OC3-VR105	NC	-	11K	NC	Infinite	NC	11K	NC	
XV10	OC3-VR105	NC	Infinite	11K	NC	c.50K	NC	11K	NC	
XV11	12AU7	22K	1.1 meg.	35K	-	-	12K	c.50K	35K	.05
XV12	12AX7	300K	1 meg.	-	-	-	110K	1 meg.**	700	.05
XV13	6AL5	270K	350K	-	.05	220K	12K	350K		
XV14	6C4	70K	NC	-	.05	70K	110K	2200		
XV15	12AU7	12.5K	140K	900	-	-	12.5K	140K	900	.05
XV16	6146	.65	0	c.50K	NC	d.500 to 5K	NC	-	NC	
XV17	6146	.65	0	c.50K	NC	d.500 to 5K	NC	-	NC	
XV18	866	40K	40K	20K	40K					
XV19	866	40K	NC	.2	40K					
XV20	5V4	NC	13K	13K	58	NC	60	NC	13K	
XV21	6BY5GA	37	0	NC	8.5K	8.5K	7.5K	0	38	

Note 1: Since XV1 and XV2 are not readily accessible, resistance to ground for terminals of terminal strip TS6 are listed:

Terminal	Resistance	Terminal	Resistance
1	23K	5	.7
2	.1	6	14K
3	2.25	7	2.25
4	6.5	8	100K

* approximate values resistance to chassis, may vary plus or minus 20%.
- grounded to Chassis
NC No Connection
** Audio gain at 10
a. Drive control setting
b. RF Bias control setting
c. Am position of Mode Switch
d. Mod Bias control setting

TABLE 3

TRANSFORMER AND CHOKE MEASUREMENTS

T1 - 22.1283 HIGH VOLTAGE TRANSFORMER

Leads	Open Circuit Voltages	Resistance (ohms)
Red to Red Yellow	760 V AC	50
Red to Red Yellow	760 V AC	50
Red to Red		100
Black to Black		.5

T2 - 22.1282 LOW VOLTAGE TRANSFORMER

Blue to Red Yellow	215 V AC	40
Blue to Red Yellow	215 V AC	40
Blue to Blue		80
Red to Red Yellow	310 V AC	65
Red to Red Yellow	310 V AC	65
Black to Black		1.4
Brown to Brown	2.6 V	.05
Green to Green	6.8 V	.05
Yellow to Yellow	5.4 V	.2

T3 - 22.1285 MODULATION TRANSFORMER

Blue to Brown		90
Blue to Red		45
Brown to Red		45
Yellow to Red Yellow		18
Green to Green Yellow		18

T4 - 22.1286 DRIVER TRANSFORMER

Red to Blue		230
Green to Yellow		800

L43 - 22.1284 H.V. CHOKE

Black to Black		45

L44 - 22.749 LOW VOLTAGE CHOKE

Black to Black		300

L45 - 22.1247 AUDIO REACTOR

Black to Black		900

TABLE 4

VIKING VALIANT II TRANSMITTER - TYPICAL DIAL SETTINGS*

CW MODE

OSCILLATOR - VFO
LOAD - 50 ohms (resistive)

Plate - 450 ma.
Grid - 8.0 ma.

Frequency	Band	Exciter	Final	Aux	Fine	Drive
1.80 mcs.	160	55	48	5	7.5	1
3.55 mcs.	80	48	23	3	3	2.5
7.1 mcs.	40	80	40	7	6	2.5
14.1 mcs.	20	48	34	9	5	6.5
21.15 mcs.	15	79	60	10	3	3
28.2 mcs.	10	68	70	10	5	3.5
27.0 mcs.	11	53	67	10	4.5	4.5

AM MODE

OSCILLATOR - VFO
LOAD - 50 ohms (resistive)

Plate - 330 ma.
Grid - 8.0 ma.

Frequency	Band	Exciter	Final	Aux	Fine	Drive
1.80 mcs.	160	55	46	3	1	1
3.9 mcs.	80	83	71	2	9	2.5
7.25 mcs.	40	87	58	7	1	2.5
14.25 mcs.	20	51	40	9	3	6
21.3 mcs.	15	81	63	10	2	3
29.0 mcs.	10	75	75	10	5	3
27.0 mcs.	11	53	69	10	4	3.5

* To be used only for rough approximations of correct tuning.

Band switching or changing frequency will be made considerably easier if a record is kept of the dial positions for each band or frequency used. The FINAL, AUXILIARY and FINE coupling settings will change with different antennas or loads antennas or loads at the same frequency.

VIKING VALIANT II TRANSMITTER

Parts List

Part No. or Drawing No.	Item No.	Qty.	Description
16.1001-4	BKT1-5	5	Top-chassis component mounting brackets
16.1001-5	BKT6	1	Under-chassis component counting brackets
16.1165-1	BKT7	1	Under-chassis bandswitch bracket
16.1167-2	BKT8-11	4	VFO cond. brackets
16.82-22	BKT12	1	Bracket, loading capacitor mounting
22.1155-2	BKT13	1	Meter shield bracket
16.82-23	BKT14	1	L bracket, plate blocking condenser
16.82-24	BKT15, 16	2	L bracket VFO stiffener
169-26	C1A, B	1	Special LA dual variable condenser
160-107-51	C2, 5	2	15M11 variable condenser
160-107-50	C4	1	15M11 variable condenser
160-130-50	C6, 3	2	30M8 variable condenser
149-3-3	C7	1	50R12 variable condenser
149-530-3	C8A, B	1	12ORD18 variable condenser
149-13-3	C9	1	360R12 variable condenser
22.1893	C10	1	11 ±5% mmf N470 500 V disc ceramic condenser
22.954	C11	1	62 2 1/2% mmf NPO 500 V ceramic condenser
22.804	C12, 13, 76	3	500 2% mmf 500 V silver mica condenser
22.805	C14, 15, 35, 94, 95	5	1000 2% mmf 500 V silver mica condenser
22.809	C16	1	91 2 1/2% mmf N080 ceramic condenser
22.823	C17	1	140 2 1/2% mmf NPO 500 V ceramic condenser
22.807	C18	1	43 2 1/2% mmf NPO 500 V ceramic condenser
22.827	C19-21, 25-28, 30, 31, 33, 34, 36, 49-53, 57, 59-73, 86, 88, 103, 104	37	.005 mfd 600 V GMV ceramic condenser
22.774	C22, 77	2	300 mmf 500 V 20% mica condenser
22.777	C23, 96, 97	3	25 mmf 500 V 5% silver mica condenser
22.862	C24, 80	2	200 mmf 500 V 20% mica condenser
22.776	C29, 105	2	50 mmf 500 V 5% silver mica condenser
22.1112	C37	1	500 mmfd 20 KV trans. type condenser
23.1626-1	C38	1	150 mmf 5% capacitor assembly
23.1626-2	C39	1	350 mmf 5% capacitor assembly
22.1446	C42	1	620 mmf 1200 WV mica condenser
22.1448	C41	1	300 mmf ±10% 1200 WV mica condenser
22.826	C47, 48, 112	3	.01 mfd 1500 V ceramic condenser
22.956	C54, 55, 56, 58	4	.002 mfd 1500 V ceramic condenser
167-701-2	C74	1	10L50 neut. condenser
22.1097	C90, 79, 83, 84, 108, 109, 110, 111	8	.01 +80 -20% mfd ceramic disc condenser
22.768	C82, 85, 78, 100	4	.1 mfd 400 WV paper condenser
22.1298	C91, 92	2	80 mfd 450 V electrolytic condenser
22.1299	C93A, B	1	15-15 mfd 350 V electrolytic condenser
22.764	C98A, B	1	15-15 mfd 450 V electrolytic condenser
22.763	C99	1	10 mfd 25 V electrolytic condenser
22.828	C40	1	.001 mfd 1.5 KV ceramic condenser
22.856	C75	1	10 mmf 500 V 5% silver mica condenser
22.857	C101	1	.005 mf disc ceramic condenser
22.4035-10	C113	1	27 mmf ±10% 500 V durmica capacitor
22.1494	C114	1	12 mmf NPO 5% 600 WV disc ceramic capacitor
22.1495	C115	1	12 mmf N750 5% 600 WV disc ceramic capacitor
160-311-50	C116	1	19 mmf differential capacitor

Parts List

Part No. or Drawing No.	Item No.	Qty.	Description
22.1927	C117	1	22 mmf NPO disc ceramic capacitor
22.1866	C106	1	900 mmf ±10% 1200 WV mica capacitor
22.1867	C107	1	1200 mmf ±10% 1200 WV mica capacitor
22.1006	C89	1	.5 mfd 400 WV paper condenser
17.990	CH1	1	Chassis
23.1128-3	CH2	1	Cabinet
23.1193-6	CH3	1	Panel
17.853-2	CH4	2	Chassis rails
17.820	CH5	1	VFO Top
17.819	CH6	1	VFO Side Plate
18.699	CH7	1	VFO Phenolic Plate
17.855	CH8	1	VFO Sub-Chassis
22.1475-2	CH9	4	Button Polyethelene Rest
71.43-097	CH10	65"	3/16" round Metaltex gasket
23.1059	D1	1	Drive arm for VFO switch
14.504	D2	1	Drive cam for VFO switch
23.1062	D3	1	Planetary drive assembly
17.858-6	D4	1	Dial escutcheon
22.993-5	D5	1	Dial plate
42.0361-310	D6	24"	Adhesive backed gasket
23.1064-3	D8	1	Dial pointer
23.564-56	D9B	1	Red jewel
23.564-57	D9A	1	Green jewel
13.123-12	D22	5	3/8"-32 panel bearings
13.760-2	D23	3	Couplings (Less set screws)
13.49-9	D24	2	VFO sub-chassis spacer
14.31-62	D25	2	1 3/8" crystal socket spacer
14.31-64	D27	4	2 1/8" VFO chassis rods
14.31-65	D28	4	2 15/16" VFO chassis rods
14.139-2	D30	1	6 7/16" ext. shaft
14.139-1	D31	1	5 5/16" ext. shaft
18.638-2	D32	5	VFO trimmer shafts
14.139-4	D33	1	8 1/8" ext. shaft
23.1607-22	D34	2	100-0 knob
116.223-11	D35	5	Phenolic knob, 1 1/8" with pointer
116.263-11	D36	1	1 5/8" band knob, maroon with pointer
23.1060-3	D37	1	Crystal knob cover
23.1463	D38	1	2 3/8" maroon knob
104-264-3	D39	1	Insulated shaft coupler
13.155-114	D40	2	Spacers 11/16"
13.155-87	D41	1	Spacer 7/16"
18.36-7	E1	2	5/8" O.D. x 17/64" I.D. x 3/8" fiber shoulder bushing
22.1309	E6	1	83-765 hood UG-177/U
16.35-1	E8-12	5	Tube caps
16.51-5	E13, 14	2	Tube caps
10.55-2	E15	1	Ceramic post insulator
10.19-2	E16	1	Cone insulator 1 1/2"
10.19-3	E17	1	Cone insulator 2"
16.1282	E18	1	Plate connector strap
22.950	E19	1	Coil fastener

Parts List

Part No. or Drawing No.	Item No.	Qty.	Description
22.1397	F1	1	1.6 amp fuse - Slo-Blo
22.840	F2, 3	2	8 amp fuse
22.1094	FH1	1	Fuse holder
22.113-1	G1-9	9	Grommet
22.113-5	G10	1	Grommet
23.1201	H1	1	Harness
23.1603-2	D42	3	Knob, 3/4" aluminum, with pointer
22.1896	D43	1	Nameplate
22.1896	D43	1	Nameplate
			#4 hardware envelope
			#6 hardware envelope
			#8 hardware envelope
			#10 hardware envelope
22.377	I1, 2	2	#51 pilot lamps
22.21	I3	1	6S6 117 V lamp
22.979	J1	1	Mic. jack
22.1246	J2	1	Single closed circuit jack
22.1096	J3	1	Single phono jack
126.105	J4	1	Relay jack
22.746	J5, 6	2	83-1R coax, receptacles
22.849-2	J7	1	Octal socket
22.977	J8	1	9 pin mica filled socket, octal style
22.1585	J9	1	5 pin socket jack
22.1868	J10	1	Phono jack
13.1050	J11	1	Coax. shield adaptor
13.1051	J12	1	Coax. retainer cap
23.968-2	L1A, B	1	Dual VFO coil
22.844-2	L2, 41	2	52 uh rf choke
22.1193	L3, 4, 7, 14, 15, 40	6	2.4 mh rf choke
22.949-2	L5	1	Oscillator coil
22.902-13	L6A	1	LF buffer coil
23.913-2	L6B	1	HF buffer coil
23.912-3	L8-10	3	Plate parasitic suppressors
102-754-2	L11	1	#754 choke
23.1000	L12, 18	2	4.7 uh rf choke
23.1202	L13A	1	Final tank coil
23.1203	L13B	1	Final aux; tank coil
22.1549	L46, 47	2	20 uh rf choke
23.1204	L17	1	VFO output coil variable
22.844	L19	1	RF choke (single pi) 200 uh
22.844-3	L20	1	RF choke 125 uh
23.902-12	L39	1	160 meter aux. coil
22.1284	L43	1	High voltage choke
22.749	L44	1	Low voltage choke
22.1247	L45	1	Audio reactor
22.1880	M1	1	Meter
22.1095	P3	1	Single phono plug
23.1031	P4	1	Relay plug
22.978	P8	1	9 pin plug
22.981	P9	1	Fused power plug
22.1731	P10	1	5 pin plug
22.5097-10	R1, 37	2	100K 1/2 watt carbon resistor 10%
22.5019-10	R2, 64	2	56 ohm 1/2 watt carbon resistor 10%

Parts List

Part No. or Drawing No.	Item No.	Qty.	Description
22.7079-10	R3, 20, 41	3	18 K 2 watt carbon resistor 10%
22.6053-10	R4	1	1.5K 1 watt carbon resistor 10%
22.5041-10	R5	1	470 ohm 1/2 watt carbon resistor 10%
22.7101-10	R6	1	150K ohm ±10% 2 W carbon resistor
22.5121-10	R7, 25, 40, 65, 66	5	1 meg 1/2 watt carbon resistor 10%
22.7099-10	R8	1	120 2 watt carbon resistor 10%
22.6077-10	R9	1	15K 1 watt carbon resistor 10%
22.7025-10	R10, 54	2	100 ohm 2 watt carbon resistor 10%
22.5085-10	R12	1	33K 1/2 watt carbon resistor 10%
22.832	R13	1	1 meg 1/2 watt potentiometer
22.6097-10	R11	1	100K 1 watt carbon resistor 10%
22.5113-10	R14	1	470K 1/2 watt carbon resistor 10%
22.1288	R15	1	12K 25 watt wire wound resistor 5%
22.1310	R16	1	12K 50 watt fixed WW resistor
22.1099	R17, 18	2	20K 10 watt wire wound resistor
22.1306	R19	1	15K ±10% 10 watt resistor
22.7077-10	R21	1	15K 2 watt carbon resistor 10%
22.1293	R23	1	9K 7 watt resistor 10%
22.5065-10	R24, 36	2	4.7K 1/2 watt carbon resistor 10%
22.1195	R28	1	1 meg. 1/4 watt log taper potentiometer
22.5045-10	R29	1	680 ohm 1/2 watt carbon resistor 10%
22.5105-10	R31, 53	2	220K 1/2 watt carbon resistor 10%
22.1290	R34	1	100K 2 watt linear taper potentiometer
22.5089-10	R26, 30, 35, 52	4	47K 1/2 watt carbon resistor 10%
22.5081-10	R38	1	22K 1/2 watt carbon resistor 10%
22.1115	R39	1	100K 1/2 watt linear potentiometer
22.5101-10	R43, 22	2	150K 1/2 watt carbon resistor 10%
22.5057-10	R44	1	2.2K 1/2 watt carbon resistor 10%
22.5047-10	R45	1	820 ohm 1/2 watt carbon resistor 10%
22.5025-10	R46, 47	2	100 ohm 1/2 watt carbon resistor 10%
22.5009-10	R48, 49	2	22 ohm 1/2 watt carbon resistor 10%
22.7049-10	R50	1	1000 ohm 2 watt carbon resistor 10%
22.732	R51	1	25K 4 watt wire wound potentiometer
22.8033-10	R55, 56	2	2.2 ohm 5% shunt
22.8042-5	R57	1	5.1 ohm 5% shunt
22.1780	R58	1	.2021 ±5% PW2 W.W. resistance
22.1781	R59	1	.4042 ±5% PW2 W.W. resistance
22.1395	R61	1	5K 2 watt potentiometer 10%
22.1396	R62	1	5K 4 watt potentiometer 10%
22.9108-5	R63	1	15K 7 watt wire wound resistor 5%
22.7041-10	R60	1	470 ohm 2 watt carbon resistor 10%
22.5107-10	R32	1	270K 1/2 watt carbon resistor 10%
22.5109-10	R33	1	330K 1/2 watt carbon resistor 10%
22.6089-10	R42	1	47K 1 watt carbon resistor 10%
22.1307	RY1	1	Relay DPST N.O. relay
17.981	SH1	1	Final shield
17.846	SH2	1	VFO shield
22.1154-11	SH3	1	Meter shield
17.980	SH4	1	Mic. and key shield
17.857-3	SH5	1	Buffer shield
22.948-2	SH6	1	Socket shield
22.988	SW1	1	VFO bandswitch
17.1221	SH7	1	P.A. grid shield
22.5029-1	R67	1	150 ohm ±10% 1/2 watt carbon resistor

Parts List

Part No. or Drawing No.	Item No.	Qty.	Description
22.1989	SW2	1	VFO crystal switch
22.1296	SW3	1	Bandswitch
22.1295-2	SW4	1	Mode switch
22.847-2	SW5	1	Meter switch
22.1308	SW6	1	Coupling switch
22.755	SW7, 8	2	SPST toggle switch
22.1283	T1	1	High voltage plate transformer
22.1282	T2	1	L.V. power transformer
22.1285	T3	1	Mod. transformer
22.1286	T4	1	Driver transformer
22.740-6	TS1, 10, 25	3	6 lug terminal strip
22.740-8	TS6	1	8 lug terminal strip
22.740-3	TS8, 15, 17, 32, 27, 49	7	3 lug terminal strip
22.740-7	TS12, 48	2	7 lug terminal strip
22.740-4	TS13, 18, 33	3	4 lug terminal strip
22.740-2	TS19	1	2 lug terminal strip
22.740-11	TS20	1	11 lug terminal strip
22.837	TS50, 51, 52	3	2 lug terminal strip
22.780	V1	1	6AU6 electron tube
22.787	V2	1	OA2 electron tube
22.1118	V3	1	6CL6 electron tube
22.1248	V4	1	5763 electron tube
22.788	V5, 7, 16, 17	5	6146 electron tube
22.781	V8	1	6AQ5 electron tube
22.1110	V9, 10	2	VR-105/OC3 electron tube
22.916	V11, 15	2	12AU7 tube
22.915	V12	1	12AX7 electron tube
22.786	V13	1	6AL5 electron tube
22.1249	V14	1	6C4 electron tube
22.212	V18, 19	2	866A electron tube
22.791	V20	1	5V4 electron tube
22.1332	V21	1	6BY5-GA electron tube
71.91-100	W1	16 1/2 ft.	#20 black plastic covered tinned copper wire
71.91-102	W2	9 ft.	#20 red plastic covered tinned copper wire
71.91-103	W3	2 ft.	#20 orange plastic covered tinned copper wire
71.91-104	W4	3 ft.	#20 yellow plastic covered tinned copper wire
71.91-105	W5	7 ft.	#20 green plastic covered tinned copper wire
71.91-106	W6	4 ft.	#20 blue plastic covered tinned copper wire
71.27-115	W7	11 1/2 ft.	#16 bare tinned copper wire
71.13-125	W8	45 ft.	#18 formex or nylclad copper wire
71.49-114	W9	7 ft.	Black line cord 18-2 POSJ type
22.997	W10	1/2 ft.	3/8 round wood dowel
71.32-178	W12	10"	RG59/U coaxial cable
42.24-050	W13	1 1/3 ft.	.053 I.D. varnished tubing
42.24-107	W14	1/2 ft.	.133 I.D. varnished tubing
42.24-113	W15	1/2 ft.	.208 I.D. black vinylite tubing
71.49-107	W16	3 ft.	HV wire
42.24-112	W17	1/3 ft.	#5.187 I.D. vinylite tubing, white
42.24-105	W19	1/2 ft.	#10.106 I.D. extruded black tubing XTE-30
71.0321-810	W20	15 3/4"	RG62/U coaxial cable
23.1047	XI1, 2	2	Lamp socket assembly
23.631	XI3	1	Socket assembly candelabra screw base

VIKING VALIANT II TRANSMITTER

Parts List

Part No. or Drawing No.	Item No.	Qty.	Description
23.566-3	XI4	1	Lamp socket, bayonet
22.975	XV1, 2, 8, 13, 14	5	7 pin min. mica filled socket
22.1274	XV5, 7, 9, 10, 16, 17, 20, 21	9	8 pin octal mica filled socket
22.1223	XV18, 19	2	4 pin socket

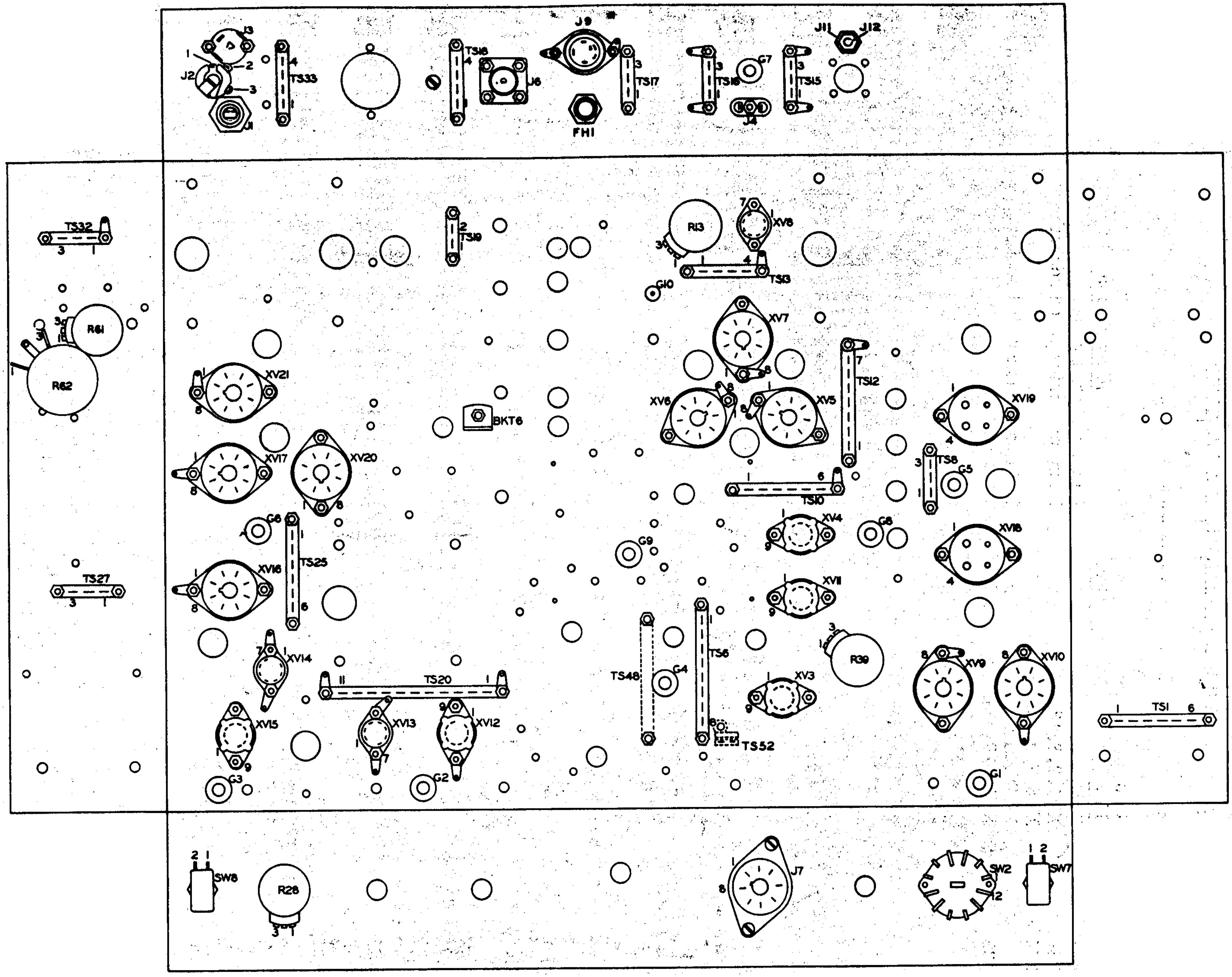


Figure 1, Valiant II Tube Layout Guide

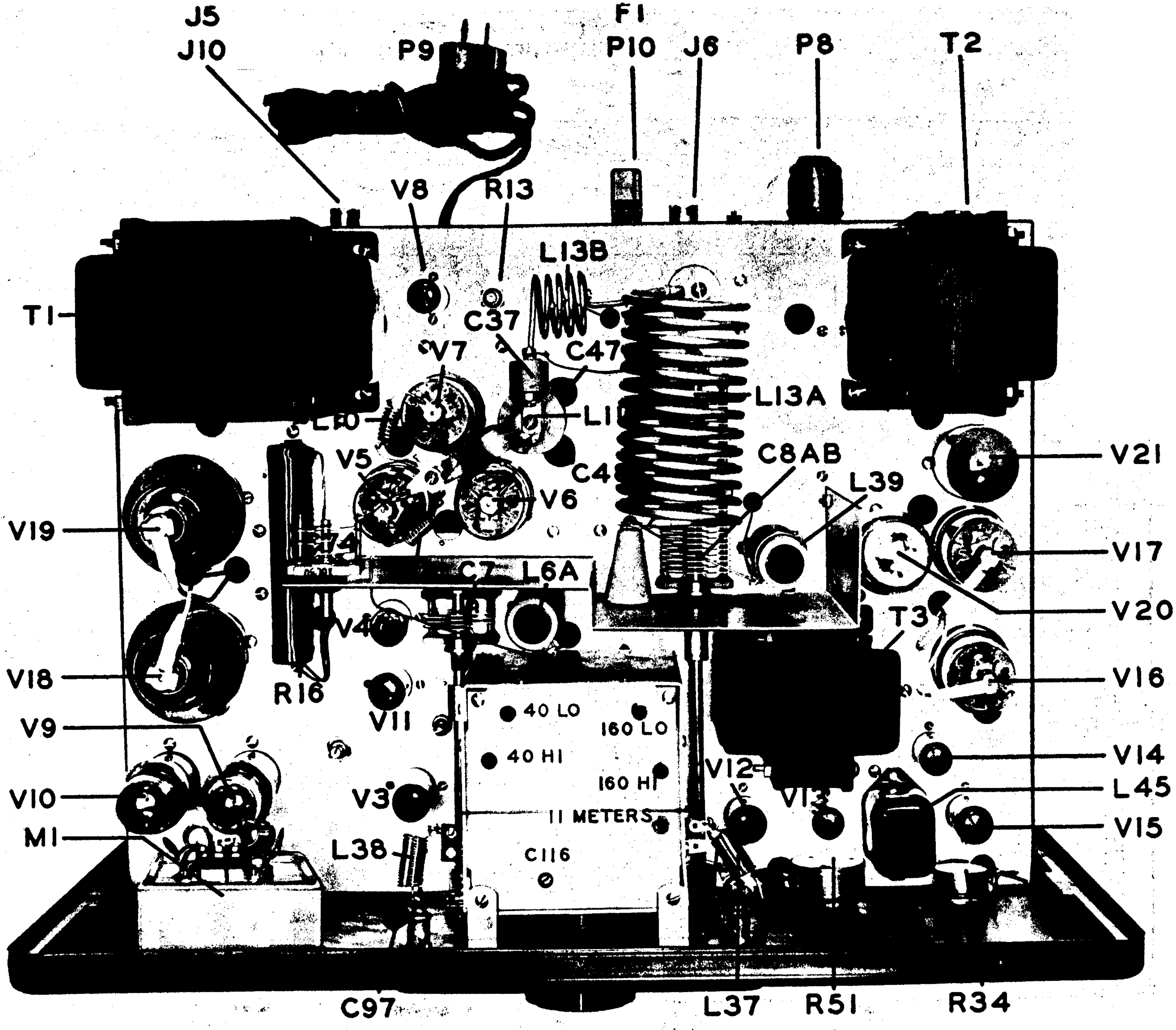


Figure 2, Valiant II, Top View

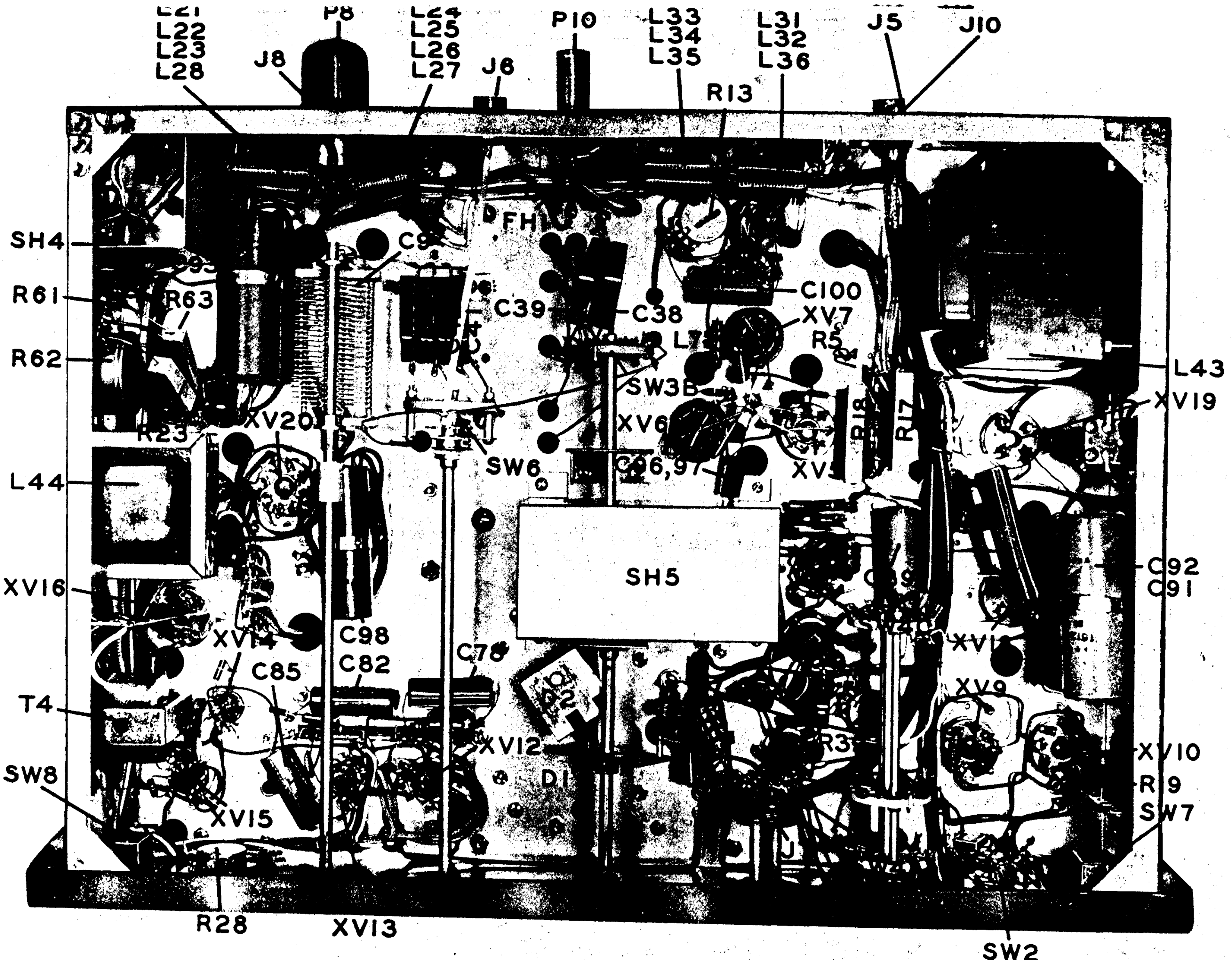


Figure 3, Valiant II, Bottom View

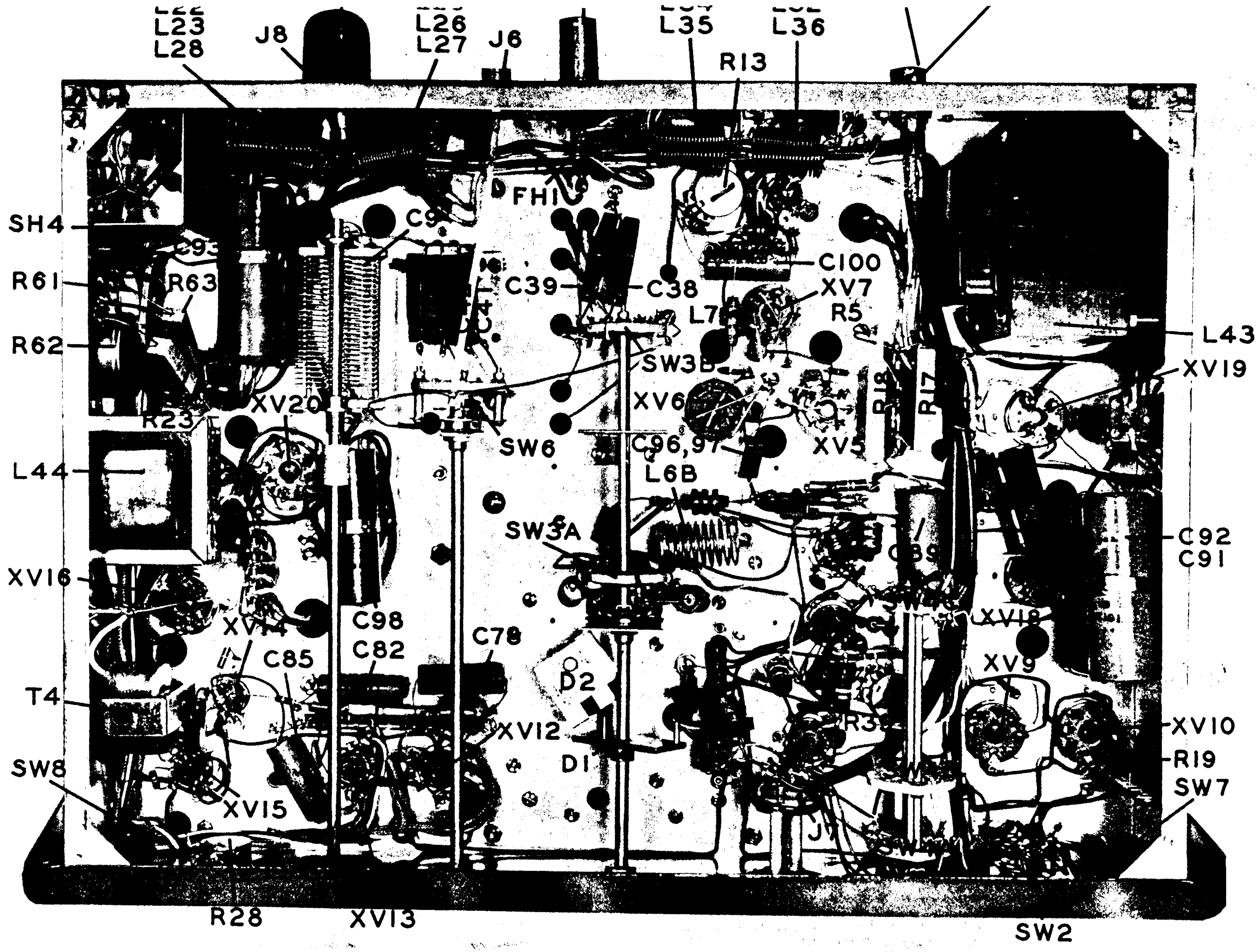


Figure 4, Valiant II, Bottom View

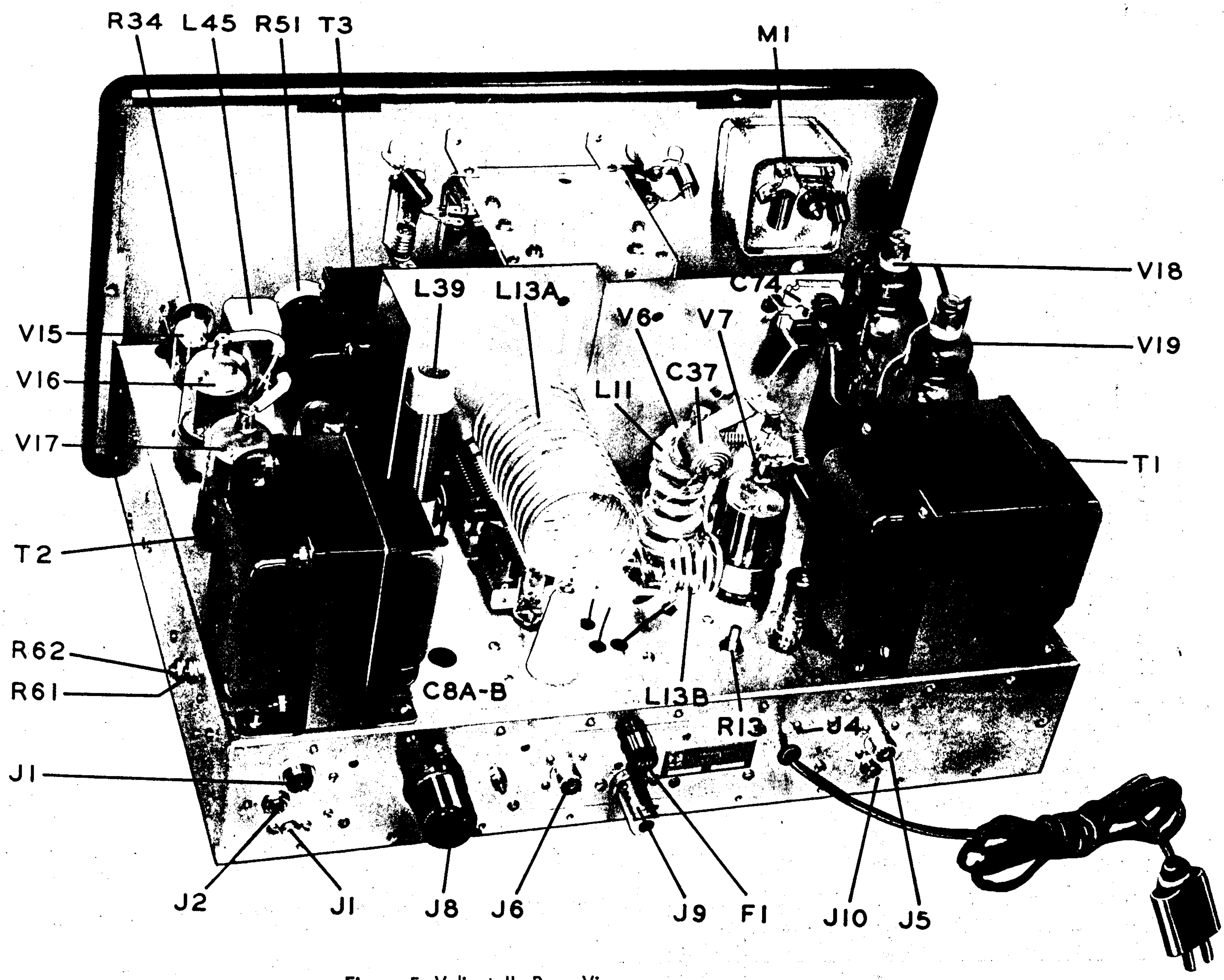


Figure 5, Valiant II, Rear View

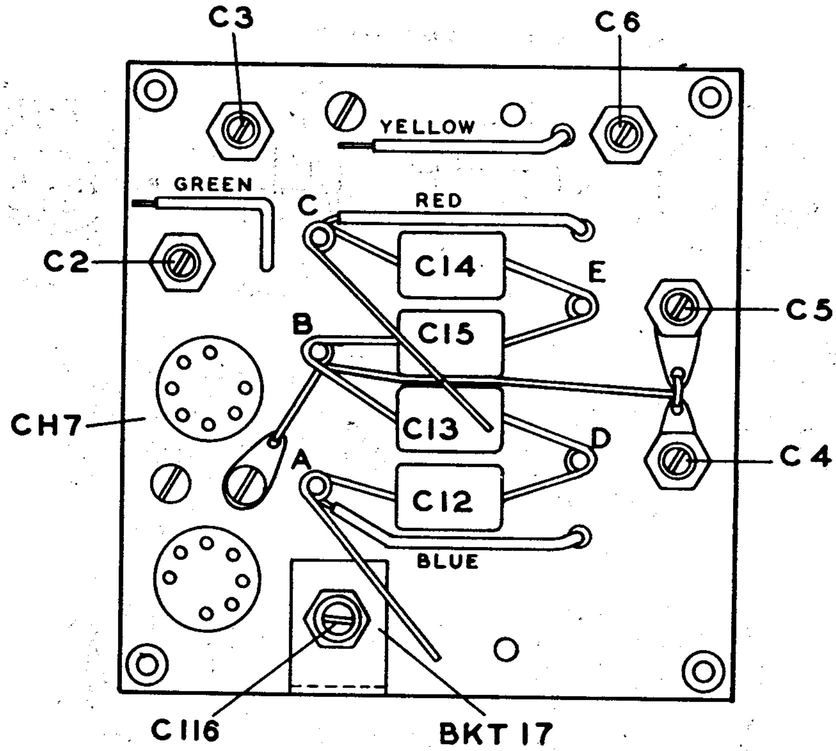


Figure 6a, VFO, Top View

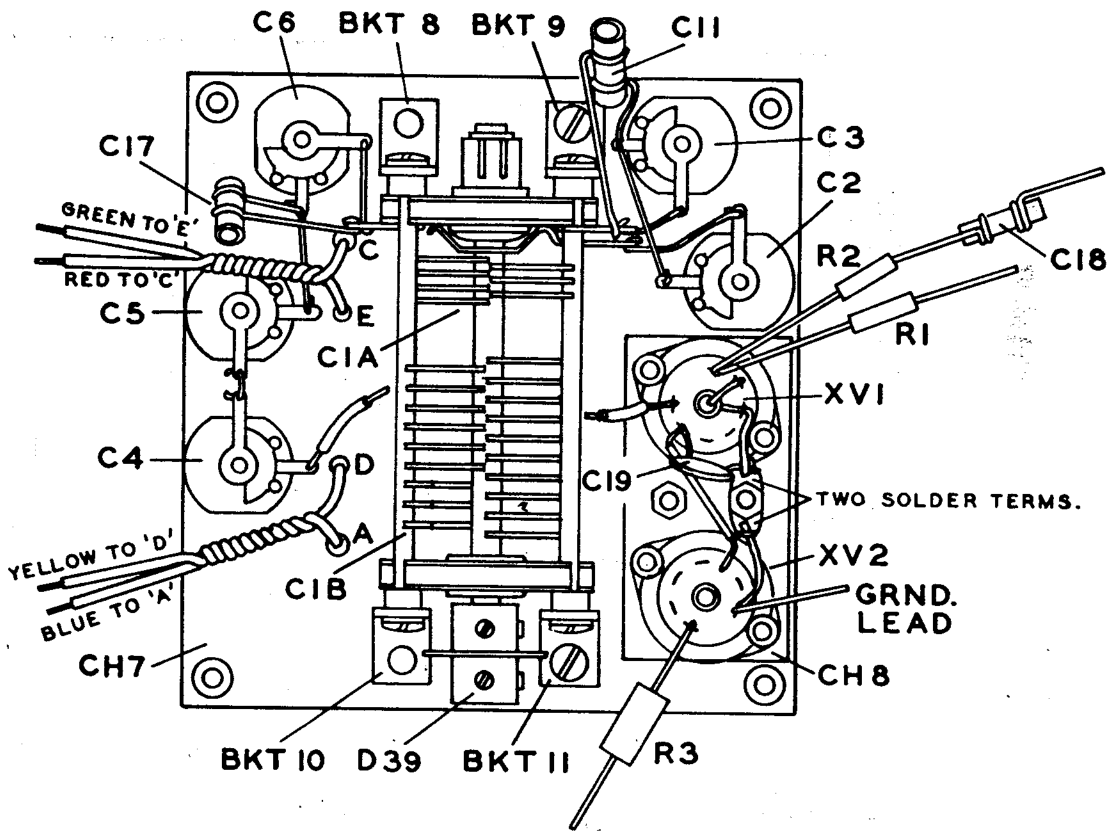
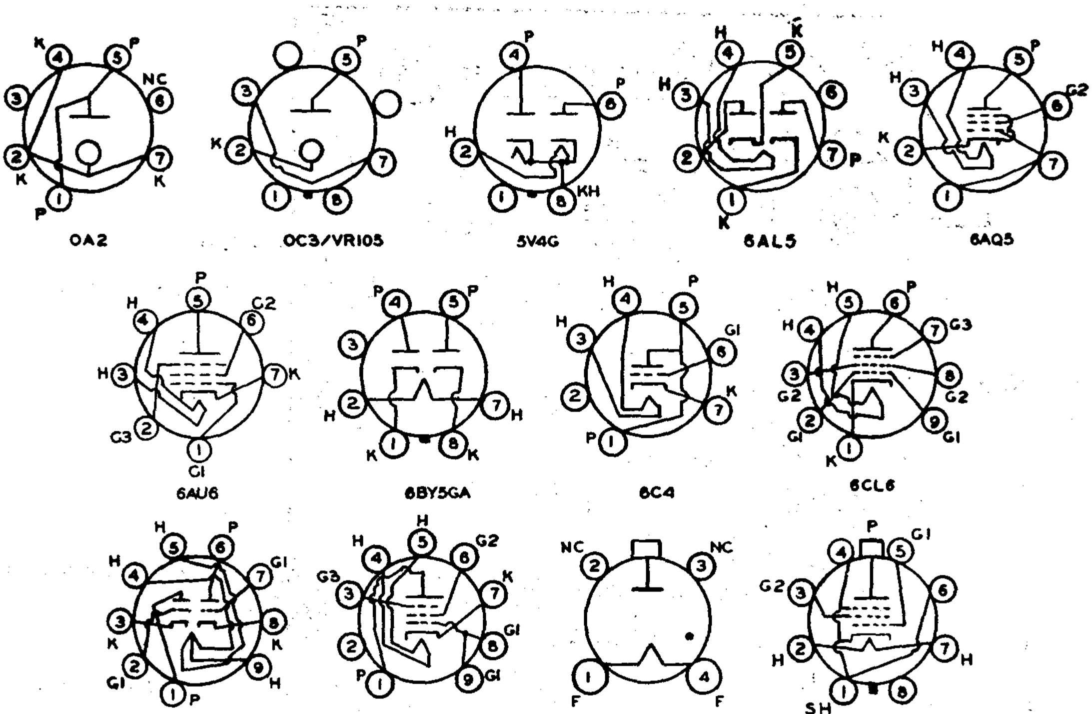


Figure 6b, VFO, Bottom View

TUBE SOCKET CONNECTIONS BOTTOM VIEW



P PLATE
K CATHODE
H HEATER
SH SHIELD OR SHELL
G1 CONTROL GRID
G2 SCREEN GRID
G3 SUPPRESSOR GRID

Figure 7a

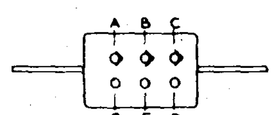
CONDENSER-RESISTOR COLOR CODE

COLOR	SIGNIFICANT FIGURE	DECIMAL MULTIPLIER	TOLERANCE (%)	VOLTAGE RATING*
BLACK	0	1	—	—
BROWN	1	10	1	100
RED	2	100	2	200
ORANGE	3	1,000	3	300
YELLOW	4	10,000	4	400
GREEN	5	100,000	5	500
BLUE	6	1,000,000	6	600
VIOLET	7	10,000,000	7	700
GRAY	8	100,000,000	8	800
WHITE	9	1,000,000,000	9	900
GOLD	-	0.1	5	1,000
SILVER	-	0.01	10	2,000
NO COLOR	-	—	20	500

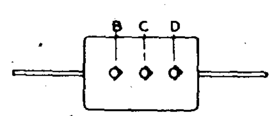
* APPLIES TO CONDENSERS ONLY

COLOR CODING OF FIXED RESISTORS

A-FIRST SIGNIFICANT FIGURE OF RESISTANCE IN OHMS
B-SECOND SIGNIFICANT FIGURE
C-DECIMAL MULTIPLIER
D-RESISTANCE TOLERANCE IN PERCENT IF NO COLOR SHOWN TOLERANCE IS ± 20%.

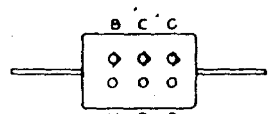


JAN FIXED CAPACITORS



RMA 3-DOT CODE 500VOLT ± 20%.

COLOR CODING OF FIXED CONDENSERS
A-TYPE MICA BLACK, PAPER SILVER
B-FIRST SIGNIFICANT FIGURE OF CAPACITY
C-SECOND SIGNIFICANT FIGURE
D-DECIMAL MULTIPLIER
E-TOLERANCE
F-CHARACTERISTIC
G-THIRD SIGNIFICANT FIGURE
H-VOLTAGE RATING



RMA 6-DOT CODE

Figure 7b

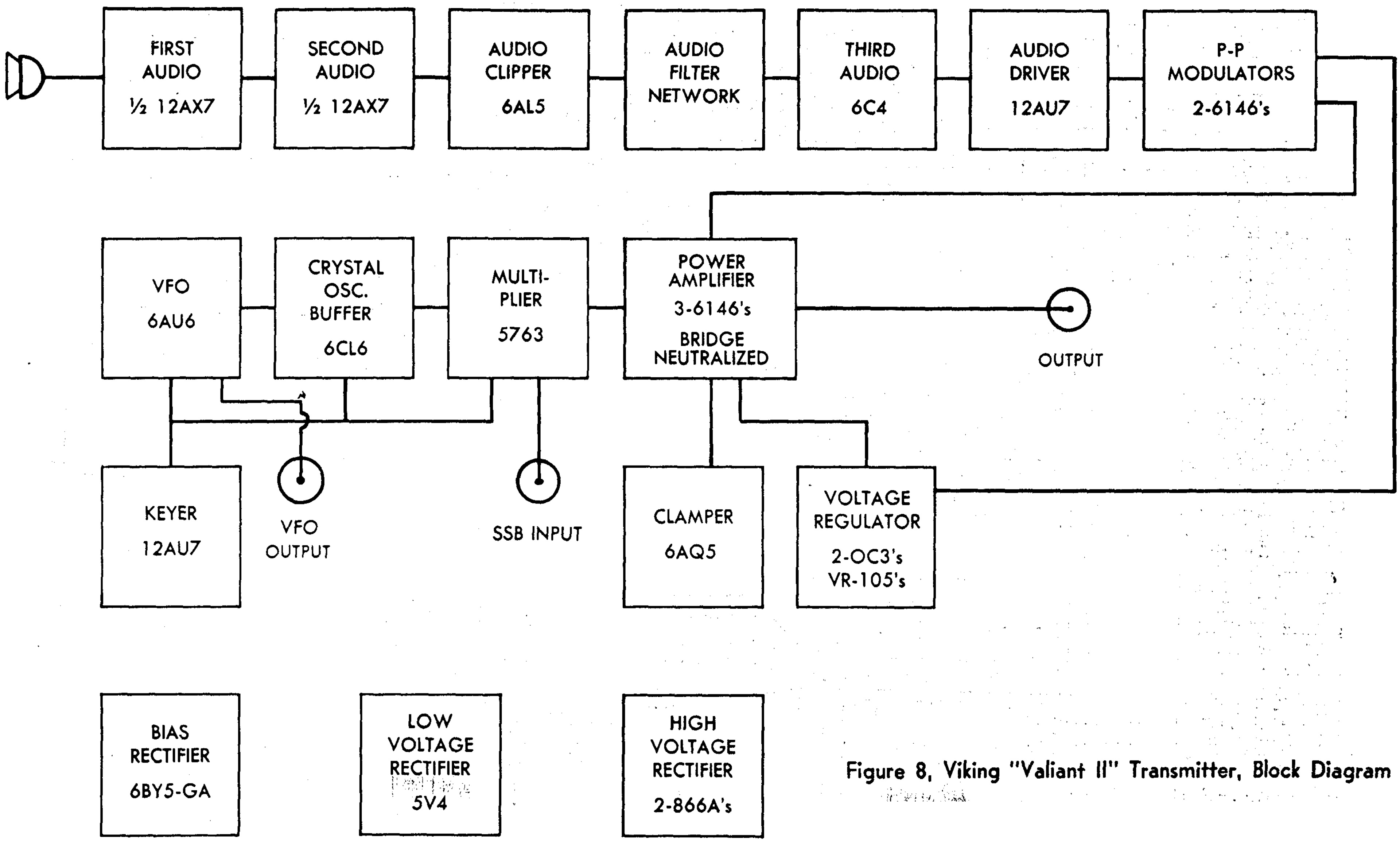
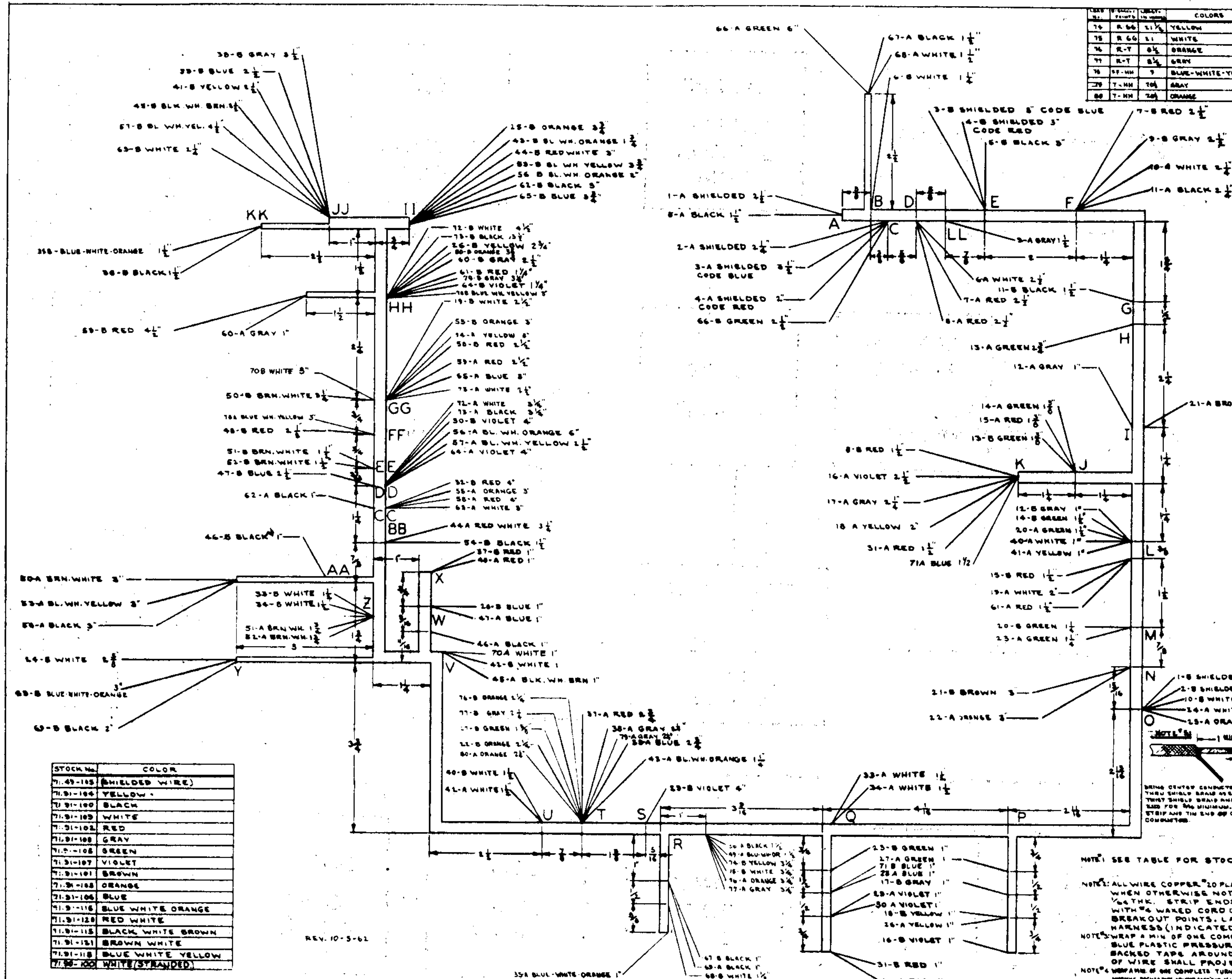


Figure 8, Viking "Valiant II" Transmitter, Block Diagram



LEAD NO.	BREAKOUT POINTS	LENGTH IN INCHES	COLORS
74	R-GG	21 1/2	YELLOW
75	R-GG	21	WHITE
76	R-T	8 1/2	ORANGE
77	R-T	8 1/2	GRAY
78	FF-HH	9	BLUE-WHITE-YELLOW
79	T-HH	20 1/2	GRAY
80	T-HH	20 1/2	ORANGE

LEAD NO.	BREAKOUT POINTS	LENGTH IN INCHES	COLORS
	A-O	22 1/2	SHIELDED WIRE
2	C-O	25	SHIELDED WIRE
3	C-E	9 1/2	SHIELDED WIRE CODE BLUE SEE NOTE 4
4	C-E	9 1/2	SHIELDED WIRE CODE RED, SEE NOTE 4
5	A-E	8	BLACK
6	D-B	5 1/4	WHITE
7	D-F	9	RED
8	D-K	17	RED
9	LL-F	7	GRAY
10	F-O	19 1/2	WHITE
11	F-G	7	BLACK
12	L-I	4 1/2	GRAY
13	H-J	6 1/2	GREEN
14	L-J	6 1/2	GREEN
15	J-L	6 1/2	RED
16	P-K	13 1/2	VIOLET
17	P-K	17 1/2	GRAY
18	P-K	17 1/2	YELLOW
19	L-GG	35 1/4	WHITE
20	L-M	4 1/2	GREEN
21	I-N	10 1/2	BROWN
22	N-T	21	ORANGE
23	Q-M	14	GREEN
24	O-Y	38 1/2	WHITE
25	O-II	38 1/2	ORANGE
26	P-HH	30 3/4	YELLOW
27	P-T	13	GREEN
28	Q-W	17	BLUE
29	Q-S	10 1/2	VIOLET
30	Q-DD	23 1/2	VIOLET
31	Q-K	21 1/2	RED
32	Q-CC	23 1/2	RED
33	Q-Z	17	WHITE-STRANDED
34	Q-Z	17	WHITE-STRANDED
35	R-KK	26 1/2	BLUE-WHITE ORANGE
36	R-KK	25 1/2	BLACK
37	T-X	12 1/2	RED
38	T-JJ	24 1/2	GRAY
39	T-JJ	23 1/2	BLUE
40	L-U	22	WHITE
41	L-JJ	40	YELLOW
42	U-V	6 1/2	WHITE
43	T-II	21	BLUE WHITE ORANGE
44	BB-II	14	RED WHITE
45	V-JJ	15	BLACK WH. BROWN
46	W-AA	7	BLACK
47	W-DD	9 1/2	BLUE
48	X-FF	11 1/2	RED
49	R-Y	18 1/2	BLUE-WHITE ORANGE
50	AA-GG	13 1/2	BROWN WH[illegible]E
51	Z-EE	6 1/2	BROWN WHITE
52	Z-EE	6 1/2	BROWN WHITE
53	AA-II	18 1/2	BLUE WHITE YELLOW
54	AA-BB	9	BLACK
55	CC-GG	8 1/2	ORANGE
56	DD-II	14 1/2	BLUE WHITE ORANGE
57	DD-JJ	14	BLUE WHITE YELLOW
58	CC-GG	9 1/2	RED
59	GG-HH	11 1/2	RED
60	HH-KK	6 1/2	GRAY
61	L-HH	36 1/2	RED
62	CC-II	11 1/2	BLACK
63	CC-JJ	13	WHITE
64	DD-HH	9 1/2	VIOLET
65	GG-II	11 1/2	BLUE
66	B-C	12	GREEN
67	B-R	35 1/2	BLACK
68	B-R	36	WHITE
69	R-Y	18	BLACK
70	V-GG	11	WHITE
71	K-Q	21	BLUE
72	DD-HH	12 1/2	WHITE
73	DD-HH	11 1/2	BLACK

STOCK No.	COLOR
71.49-145	SHIELDED WIRE
71.91-104	YELLOW
71.91-100	BLACK
71.91-103	WHITE
71.31-102	RED
71.91-108	GRAY
71.9-105	GREEN
71.31-107	VIOLET
71.31-101	BROWN
71.31-103	ORANGE
71.31-106	BLUE
71.9-116	BLUE WHITE ORANGE
71.91-120	RED WHITE
71.91-115	BLACK WHITE BROWN
71.91-121	BROWN WHITE
71.91-118	BLUE WHITE YELLOW
71.96-100	WHITE (STRANDED)

NOTE 1: SEE TABLE FOR STOCK NUMBERS.

NOTE 2: ALL WIRE COPPER #20 PLASTIC COATED (EXCEPT WHEN OTHERWISE NOTED). PLASTIC COATING 1/64 THK. STRIP ENDS 5/16". LACE HARNESS WITH #4 WAXED CORD OR TAPE. DOUBLE AT ALL BREAKOUT POINTS. LACE MAIN PARTS OF HARNESS (INDICATED BY DOUBLE LINE).

NOTE 3: WRAP A MIN OF ONE COMPLETE TURN OF 1/2 MIN WIDTH BLUE PLASTIC PRESSURE SENSITIVE ADHESIVE BACKED TAPE AROUND EACH END OF LEAD; 1" TO 1 1/4" OF WIRE SHALL PROJECT BEYOND TAPE.

NOTE 4: [illegible]

REV. 10-5-62

Figure 10, Valiant II Wiring Harness

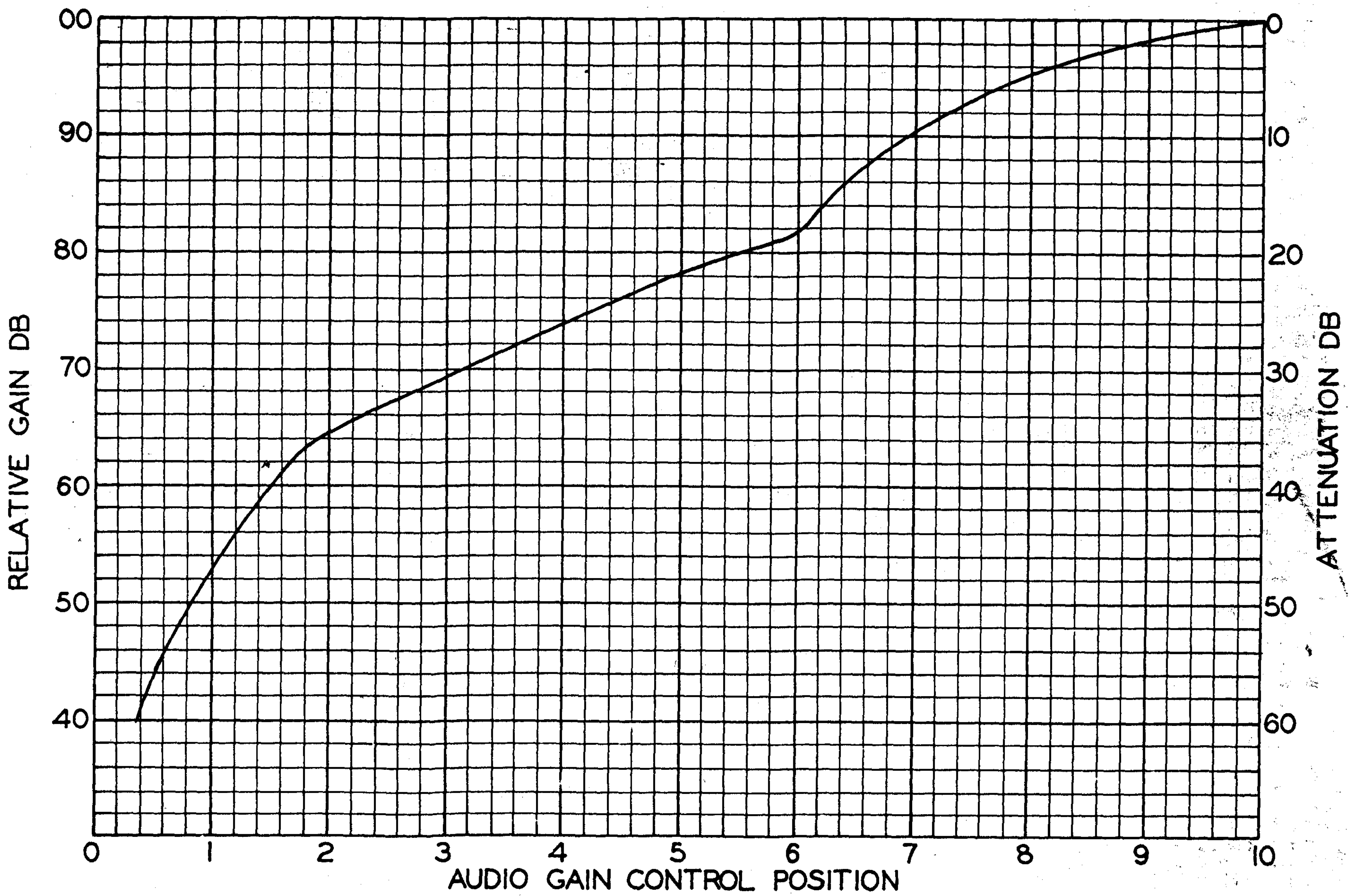
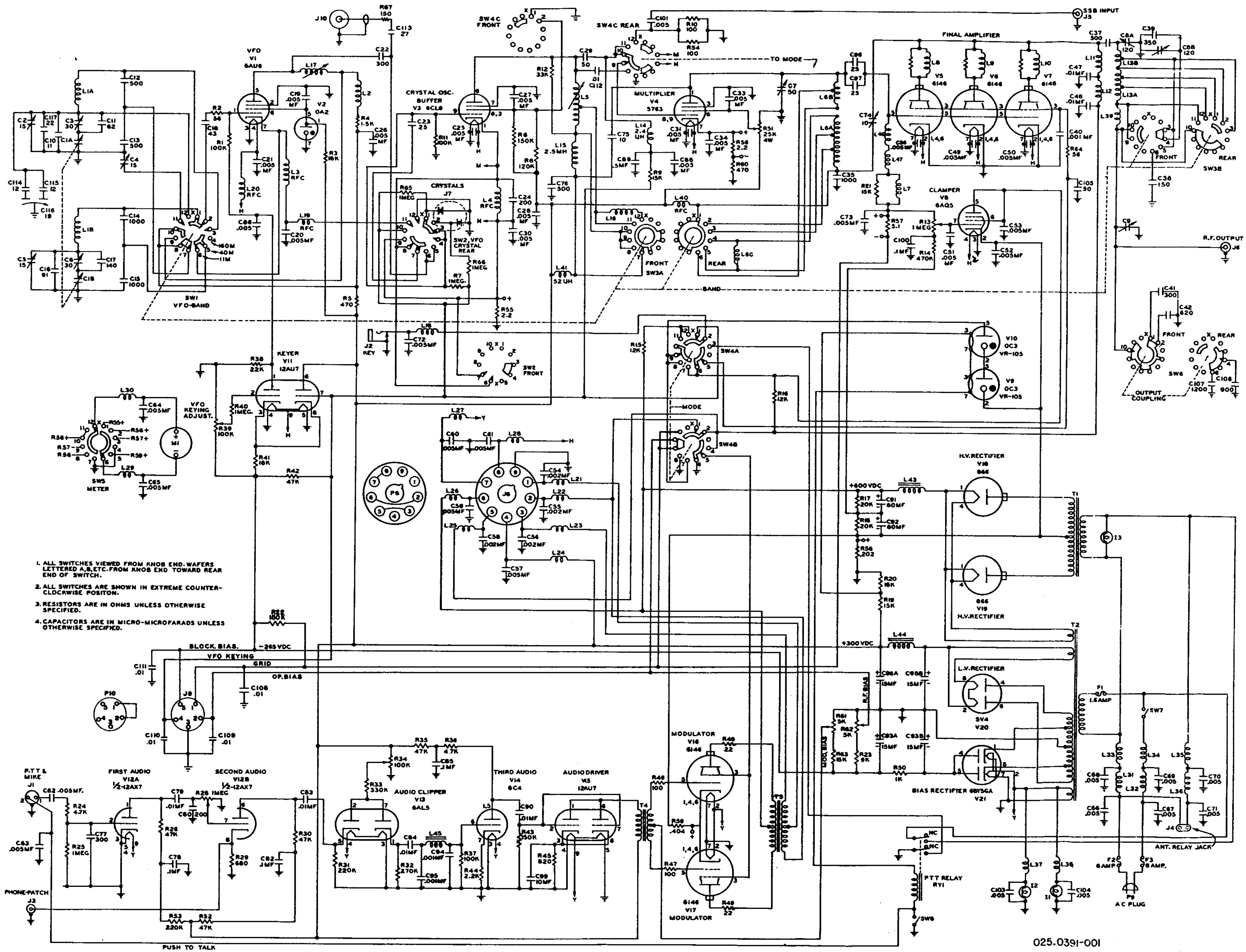


Figure 11, Audio Gain Control Curve



1. ALL SWITCHES VIEWED FROM KNOB END. WAFERS LETTERED A,B,ETC. FROM KNOB END TOWARD REAR END OF SWITCH.

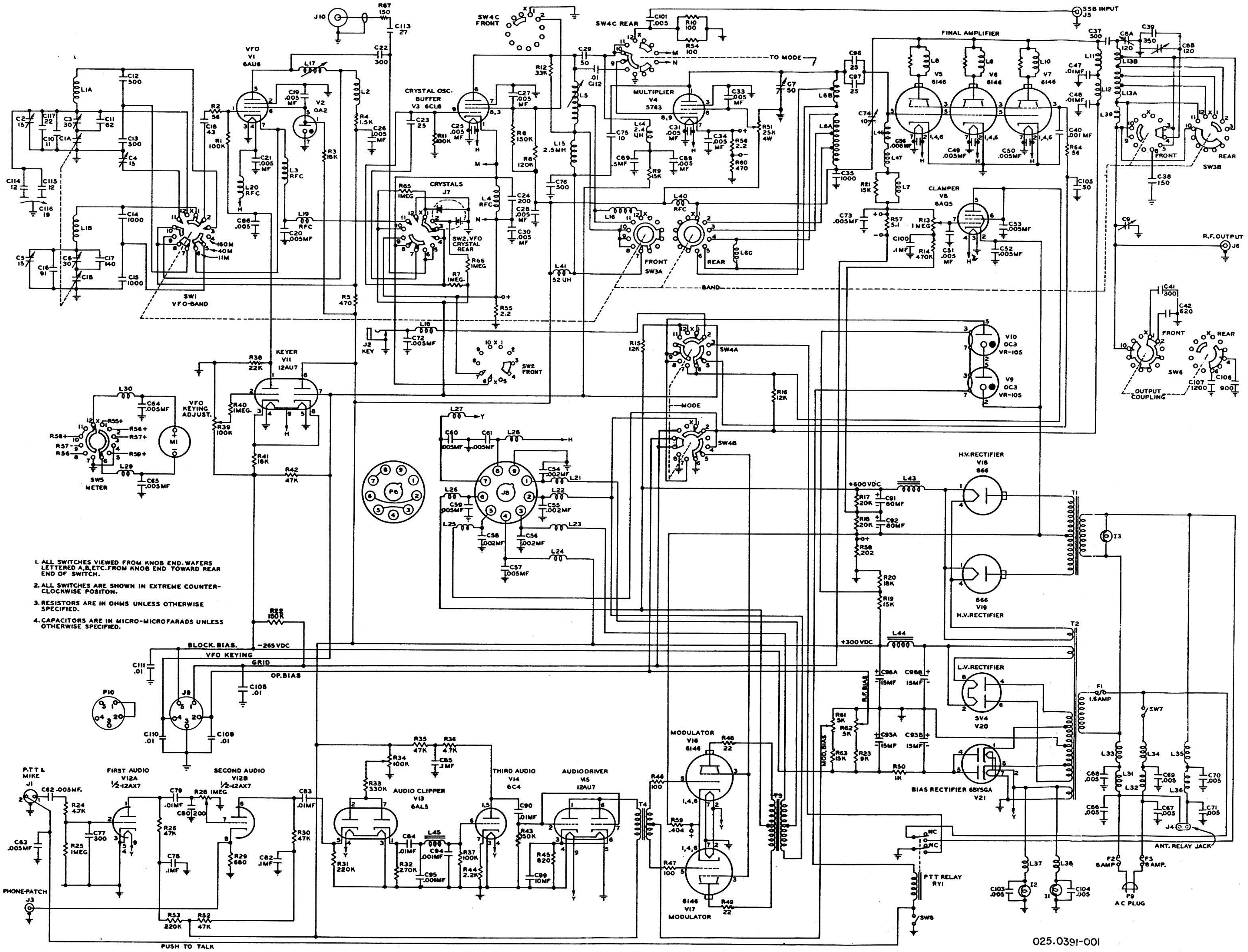
2. ALL SWITCHES ARE SHOWN IN EXTREME COUNTER-CLOCKWISE POSITON.

3. RESISTORS ARE IN OHMS UNLESS OTHERWISE SPECIFIED.

4. CAPACITORS ARE IN MICRO-MICROFARADS UNLESS OTHERWISE SPECIFIED.

025.0391-001

REVISED 4-2-63



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